

Soret and Angle of Inclination Effects on MHD Fluid Flow Past an Upright Porous Plate

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Abstract:

A theoretical investigation of MHD fluid flow is carried out under the influence of thermal diffusion, chemical reaction, and various factors. The angle of inclination is also taken into account and quantitatively analyzed in this heat and mass transport analysis. The necessary governing equations are numerically resolved using the implicit finite-difference methodology of the Crank-Nicolson type. Graphs depict non-dimensional velocity, fluid temperature and concentration distributions for many fluid parameters involved, such as the joule-heating parameter, suction parameter, chemical reaction parameter, and radiation parameter. The coefficient of skin friction, Nusselt number, and Sherwood number were calculated. The concentration of the fluid increases as the Soret number increases, whereas the Sherwood number decreases.

Keywords: Magnetohydrodynamic, Heat and mass transfer, Soret effect, Angle of inclination, Implicit finite difference scheme.

Introduction

Researchers are very interested in the studies on MHD flows under various geometries because of its importance in Engineering and chemical industries. Zhang et al. [1] evaluated nanofluids' magnetohydrodynamic flow and radiation heat transfer in porous media with variable surface heat flux and chemical reaction. MHD variable viscosity reacting flow over a convectively warmed plate in a porous media with thermophoresis and radiative heat transfer was explained by Makinde et al. [2]. Heat generation/absorption on MHD stagnation flow of nanofluid towards a porous extended sheet with prescribed surface heat flux has been defined by Jalilpour et al. [3]. Raju, Raju et al. [4] examined double solutions for the flow of a nanofluid over a nonlinearly permeable extended sheet in three dimensions. Eddy, the development in film flow down a vertical plate has been clarified by Portalski [5]. Buoyancy-induced flow of non-Newtonian fluids over a non-isothermal horizontal plate embedded in a porous media, Mehta [6]. Takhar et al. [7] analyses the unsteady free convection flow across an infinite vertical porous plate as a result of the combined effects of heat and mass diffusion and a magnetic field. Makinde [8] explained free convection flow with thermal radiation and mass transfer past a moving vertical porous plate with thermal radiation and mass transfer. Chamkha et al. [9] introduced the effect of heat generation or absorption on the thermophoretic free convection boundary layer generated from a vertical flat plate embedded in a porous medium. Mahmoud [10] explained heating the radiation effect on unsteady MHD free convection flow past a vertical plate with temperature-dependent viscosity. Siddiqua et al. [11] identified radiation effects on natural convection

flow over an inclined flat plate with temperature-dependent viscosity. Raju et al. [12] explained the Impacts of an aligned magnetic field and radiation on the flow of ferrofluids over a flat plate with a non-uniform heat source/sink. Khan et al. [13] investigated the flow and heat transfer of ferrofluids over a flat plate with uniform heat flux. Benazir et al. [14] explained the unsteady magnetohydrodynamic Casson fluid flow over a vertical cone and flat plate with a non-uniform heat source/sink.

The current examination is to extend the work of Uwanta and Sani [15] by adding the Soret effect so that systems of equations are coupled. The angle of inclination is also taken as a novelty in this analysis with heat and mass transfer and analyzed numerically. The second-order partial differential equations with boundary conditions are resolved by an implicit finite-difference scheme. The impact of different parameters on non-dimensional parameters, which are velocity, temperature, and fluid concentration of flow, was conferred through figures. The skin friction coefficient and numbers of Nusselt and Sherwood were observed through tables.

OBJECTIVES: An incompressible, unsteady, electrically conducting, radiating, heat-absorbing, two-dimensional fluid flow is considered past an infinite porous vertical plate. Let the x -axis be taken along the vertical plate towards the upward direction, and the y -axis is normal to it. The magnetic field B_0 is presumed to be acting in the perpendicular direction of the fluid flow. The presence of Soret effect is also considered. Since the length of the plate is infinite, the basic fluid parameters depend on the time t and space coordinates y only. At the time $t \leq 0$, both fluid and plate are maintained at the same temperature T_∞ and concentration at all points respectively. For a time $t > 0$, the plate moves imprudently in its plane with a velocity u , also the fluid temperature and concentration at the plate are upraised to T_w and C_w respectively. Based on the above suppositions and the Boussinesq's approximation, the resultant fluid flow equations, i.e., continuity, momentum, mass-energy, and concentration (Sharma et al. 2005, Ahmed et al. 2013), respectively are given below:

$$\frac{\partial v}{\partial y} = 0 \tag{1}$$

$$\frac{\partial u}{\partial t} + v \frac{\partial u}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2} - \frac{\sigma B_0^2 u}{\rho} - \frac{v u}{K} + g \beta \cos \phi (\bar{C} - \bar{C}_\infty) + g \beta \cos \phi (\bar{T} - \bar{T}_\infty) - b_1 \bar{u}^2 \tag{2}$$

$$\frac{\partial \bar{T}}{\partial t} + v \frac{\partial \bar{T}}{\partial y} = \frac{1}{\rho C_p} \frac{\partial}{\partial y} \left(K(\bar{T}) \frac{\partial \bar{T}}{\partial y} \right) - \frac{1}{\rho C_p} \frac{\partial q_r}{\partial y} + \frac{v}{C_p} \left(\frac{\partial u}{\partial y} \right)^2 + b_2 \bar{u}^2 - \frac{Q}{\rho C_p} (\bar{T} - \bar{T}_\infty) \tag{3}$$

$$\frac{\partial \bar{C}}{\partial t} + v \frac{\partial \bar{C}}{\partial y} = D_M \frac{\partial^2 \bar{C}}{\partial y^2} + D_T \frac{\partial^2 \bar{T}}{\partial y^2} - \bar{R} (\bar{C} - \bar{C}_\infty)^n \tag{4}$$

The following initial & boundary conditions are

$$\begin{aligned} t \leq 0, \quad u(\bar{y}, t) = 0, \bar{T}(\bar{y}, t) = \bar{T}_\infty, \bar{C}(\bar{y}, t) = \bar{C}_\infty \text{ for all } \bar{y} < 0 \\ t > 0, \quad u(\bar{y}, t) = 0, \bar{T}(\bar{y}, t) = \bar{T}_w, \bar{C}(\bar{y}, t) = \bar{C}_w \text{ at } \bar{y} = 0 \\ u(\bar{y}, t) = 0, \bar{T}(\bar{y}, t) = \bar{T}_\infty, \bar{C}(\bar{y}, t) = \bar{C}_\infty \text{ as } \bar{y} \rightarrow \infty \end{aligned} \tag{5}$$

Where $t, Q, \bar{T}, \bar{C}, \bar{T}_\infty, \bar{C}_\infty, \bar{T}_w, \bar{C}_w, \nu, B_0, \sigma, K, \beta, b_1, \beta, g, D_T, D_M, \bar{R}, C_p, q_r, b, K(\bar{T}), \rho$ represent dimensional time, volumetric rate of heat generation, temperature of the fluid, species concentration, free stream temperature, free stream concentration, Surface Temperature, surface concentration, kinematic

viscosity, constant magnetic field intensity, Stefan Boltzmann constant, thermal expansion coefficient, Forchheimer parameter of the medium, concentration expansion coefficient, gravitational constant, thermal diffusivity coefficient, chemical molecular diffusivity coefficient, chemical reaction, specific heat at constant pressure, radiative heat flux, joule-heating parameter, the variable thermal conductivity, density. (\bar{u}, \bar{v}) represents fluid velocity corresponding \bar{x} and \bar{y} directions. The flow geometry is shown in Figure 1. The continuity Eq. (1) on integration, we get $\bar{v} = -v_0$, for any $v_0 > 0$, where v_0 is suction velocity. The radiative heat flux can be written by Rosseland approximation as

$$\frac{\partial q_r}{\partial \bar{y}} = -4\sigma\bar{a}(\bar{T}_\infty^4 - \bar{T}^4) \tag{7}$$

Now we expanding \bar{T}^4 into about \bar{T}_∞ in series form, we get

$$\bar{T}^4 \approx 4(\bar{T} - \bar{T}_\infty)\bar{T}_\infty^3 + \bar{T}_\infty^4 \approx 4\bar{T}\bar{T}_\infty^3 - 3\bar{T}_\infty^4 \tag{8}$$

The temperature-dependent variable thermal conductivity (Abel et al. 2009) is given by

$$K(\bar{T}) = [\delta(\bar{T} - \bar{T}_\infty) + 1]k_\alpha \tag{9}$$

where the k_α is the fluid thermal conductivity and δ is the constant.

Methods: The following non-dimensional variables are defined to obtain non-dimensional partial differential equations (PDE)

$$\begin{aligned} U = \frac{\bar{u}}{U_0}, y = \frac{\bar{y}U_0}{\nu}, t = \frac{\bar{t}U_0^2}{\nu}, \theta = \frac{\bar{T} - \bar{T}_\infty}{\bar{T}_w - \bar{T}_\infty}, C = \frac{\bar{C} - \bar{C}_\infty}{\bar{C}_w - \bar{C}_\infty}, \tau = \delta(\bar{T} - \bar{T}_\infty), b = \frac{\bar{b}\nu}{\bar{T}_w - \bar{T}_\infty}, \\ Sc = \frac{\nu}{D_M}, Pr = \frac{\nu\rho C_p}{k_\alpha}, Ec = \frac{U_0^2}{C_p(\bar{T}_w - \bar{T}_\infty)}, Gr = \frac{g\beta\nu(\bar{T}_w - \bar{T}_\infty)}{U_0^3}, Gc = \frac{g\beta\nu(\bar{C}_w - \bar{C}_\infty)}{U_0^3}, \\ \alpha = \frac{v_0}{U_0}, K = \frac{\bar{K}U_0^2}{\nu}, N = \frac{16\bar{a}\sigma\bar{T}_\infty^3\nu^2}{k_\alpha U_0^2}, M = \frac{\nu\sigma B_0^2}{\rho U_0^2}, b_1 = \frac{\bar{b}_1\nu}{U_0}, S = \frac{Q\nu^2}{k_\alpha U_0^2}, \\ S_0 = \frac{D_T}{\nu} \left(\frac{\bar{T}_w - \bar{T}_\infty}{\bar{C}_w - \bar{C}_\infty} \right), Kr = \frac{\nu\bar{R}(\bar{C}_w - \bar{C}_\infty)^{n-1}}{U_0^2} \end{aligned} \tag{10}$$

Where U_0 is the non-dimensional constant.

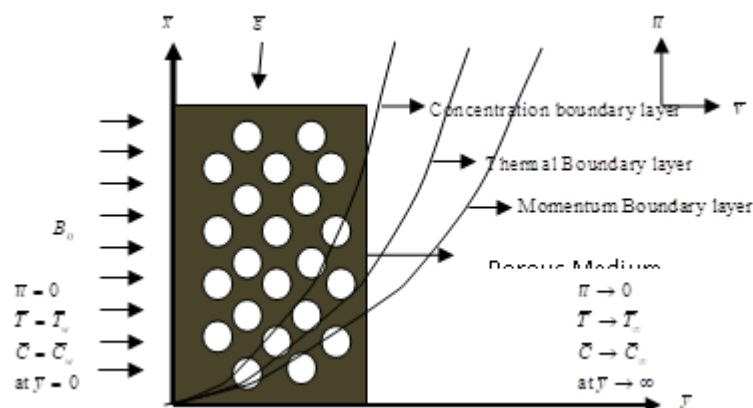


Fig. 1. Flow geometry and coordinate system

By introducing the above dimensionless variables from equation (10), then the Equations (2)-(4) converted as follows:

$$\frac{\partial U}{\partial t} - \alpha \frac{\partial U}{\partial y} = \frac{\partial^2 U}{\partial y^2} - \left(M + \frac{1}{K} \right) U + Gr \cos\phi \theta + Gc \cos\phi C - b_1 U^2 \tag{11}$$

$$\frac{\partial \theta}{\partial t} - \alpha \frac{\partial \theta}{\partial y} = \frac{(1 + \tau \theta)}{\text{Pr}} \frac{\partial^2 \theta}{\partial y^2} + \frac{\tau}{\text{Pr}} \left(\frac{\partial \theta}{\partial y} \right)^2 + \frac{(S - N)}{\text{Pr}} \theta + Ec \left(\frac{\partial U}{\partial y} \right)^2 + bU^2 \quad (12)$$

$$\frac{\partial C}{\partial t} - \alpha \frac{\partial C}{\partial y} = \frac{1}{Sc} \frac{\partial^2 C}{\partial y^2} + S_0 \frac{\partial^2 \theta}{\partial y^2} - KrC \quad (13)$$

From Eq. (5), Initial & boundary conditions are

$$\left. \begin{aligned} t \leq 0 \text{ \& } y < 0: U(y, t) = 0, \theta(y, t) = 0, C(y, t) = 0 \\ t > 0 \text{ \& } y = 0: U(y, t) = 0, \theta(y, t) = 1, C(y, t) = 1 \\ U(\infty, t) = 0, \theta(\infty, t) = 0, C(\infty, t) = 0 \end{aligned} \right\} \quad (14)$$

Where $U, \text{Pr}, b, \theta, C, Sc, Ec, Gc, M, K, N, \alpha, \tau, Kr, b, Gr, S, S_0$ represents dimensionless velocity, Prandtl number, inertia number, dimensionless temperature, dimensionless species concentration, Schmidt number, Eckert number, mass Grashof number, magnetic field, porosity, radiation, suction, variable thermal conductivity, chemical reaction, dimensionless joule-heating parameter, thermal Grashof number, heat source parameters, Soret number.

Equations (11)-(13) are 2nd order non-linear coupled PDE together with both conditions from the equation (14). So these equations (11)-(14) are resolved by using the Crank-Nicolson implicit finite-difference scheme. Therefore, finite-difference equations are mention below:

$$-r_1 U_{i-1}^{j+1} + (1 + 2r_1) U_i^{j+1} - r_1 U_{i+1}^{j+1} = r_2 U_{i-1}^j + (-r_4 - \alpha r_3 - 2r_2 + 1) U_i^j + (\alpha r_3 + r_2) U_{i+1}^j + \Delta t Gr \cos \phi \theta_i^j + Gc \cos \phi \Delta t C_i^j - b_1 \Delta t (U_i^j)^2 \quad (15)$$

$$-qr_1 \theta_{i-1}^{j+1} + (\text{Pr} + 2qr_1) \theta_i^{j+1} - qr_1 \theta_{i+1}^{j+1} = qr_2 \theta_{i-1}^j + (\text{Pr} - 2qr_2 - \alpha \text{Pr} r_3 - N \Delta t + S \Delta t) \theta_i^j + (qr_2 + \alpha \text{Pr} r_3) \theta_{i+1}^j + \tau r_5 (\theta_{i+1}^j - \theta_{i-1}^j)^2 + \text{Pr} Ec r_5 (U_{i+1}^j - U_{i-1}^j)^2 + \text{Pr} \Delta t b (U_i^j)^2 \quad (16)$$

$$-r_1 C_{i-1}^{j+1} + (Sc + 2r_1) C_i^{j+1} - r_1 C_{i+1}^{j+1} = r_2 C_{i-1}^j + (Sc - 2r_2 - \alpha Sc r_3 - Kr Sc \Delta t) C_i^j + (r_2 - \alpha r_3 Sc) C_{i+1}^j + 2Sc S_0 r_1 \theta_{i-1}^j - 4Sc S_0 r_1 \theta_i^j + 2Sc S_0 r_1 \theta_{i+1}^j \quad (17)$$

$$\text{where } r_1 = r_2 = \frac{\Delta t}{2(\Delta y)^2}, r_3 = \frac{\Delta t}{\Delta y}, r_4 = \Delta t \left(M + \frac{1}{K} \right), r_5 = \frac{\Delta t}{4(\Delta y)^2}, q = 1 + \tau \theta_i^j \quad (18)$$

Here (i, j) is an arbitrary grid point in the discrete mesh system. Where indices i & j refer to y & t respectively. The discrete mess system can be divided by rectangles whose length $\Delta y = 0.1$ and width $\Delta t = 0.001$. Also, consider $i_{\max} = 200$ and $j_{\max} = 500$. Then the equation (14) can be expressed in terms of finite-difference form for any i, j

$$\left. \begin{aligned} U(i, 0) = 0, U(0, j) = 0, U(i_{\max}, j) = 0 \\ \theta(i, 0) = 0, \theta(0, j) = 1, \theta(i_{\max}, j) = 0 \\ C(i, 0) = 0, C(0, j) = 1, C(i_{\max}, j) = 0 \end{aligned} \right\} \quad (19)$$

From the equations (15)-(17) with the above initial and boundary conditions, every internal node of each time step constitutes a tridiagonal matrix. The dimension of tridiagonal matrix is $i_{\max} - 1 \times i_{\max} - 1$. The tridiagonal matrix system of equations can be resolved by using the Thomas algorithm for solving $i_{\max} - 1$ equations with $i_{\max} - 1$ unknowns for each time step. Since it is a coupled equation, we started to compute the concentration and temperature distributions at each time step from equation (17) and

equation (16), respectively, and then calculated values are used to compute the velocity distribution at each time step from equation (15) which meets the convergence criteria. The non-dimensional parameters, which are the skin friction coefficient, Nusselt and Sherwood numbers, can be calculated by the following formulas, respectively.

$$Cf = \frac{\partial U}{\partial y}, Nu = -\frac{\partial \theta}{\partial y}, Sh = -\frac{\partial C}{\partial y} \text{ at } y=0$$

Results:

Mathematical equations are formulated and solved numerically for the problem on Soret and variable thermal conductivity effects on heat and mass transfer flow past an infinite and inclined vertical plate. The values of parameters are fixed throughout the simulations except if, in any case, expressed. That is $Gr=1.00, \tau=0.10, Sc=0.62, Kr=0.10, Ec=0.01, Pr=0.71, b=1.00, M=1.00, So=1.00, K=1.00, Gc=1.00, N=0.10, b_1=1.00, S=1.00, \alpha=1.00,$

$$n=1.00.$$

Velocity distributions are presented from Fig. 2 to Fig. 10 for diverse values of $M, K, Gr, Gc, N, \alpha, \tau, Kr, So$. Fig. 2 exhibits U for different values of $M = 1, 5, 10,$ and 15 . This figure indicates U falls with an increment in the values of M . This is because of an increment that M shows the effect on free convective flow. The variation in U with K is presented in Fig. 3. A higher permeable parameter improves the fluid velocity. Naturally, the resistance of the fluid flow might be ignored due to an increment in the size of the holes of a porous medium. The influence of α on U completely coincides with the effect of the radiation parameter as clearly observed in Fig. 4. Fig. 5 presents the effect of τ on U . It is identified fluid velocity increases with increasing τ . Figure 6 shows that the velocity decreases on increasing the angle of inclination. It is observed that θ decreases whenever α increased. Fig. 7 demonstrates θ rises with an increment in the values of τ and in the same way for Fig. 8, θ increase for the growth in the values of S .

The effect of Sc on C is presented in Fig. 9. The trend shows C reduction with augmented values of Sc due to the increase of Sc means to fall in molecular diffusion. Fig. 10 sketched the effect of α on C . It notices that the non-dimensional concentration falls with an increment of α .

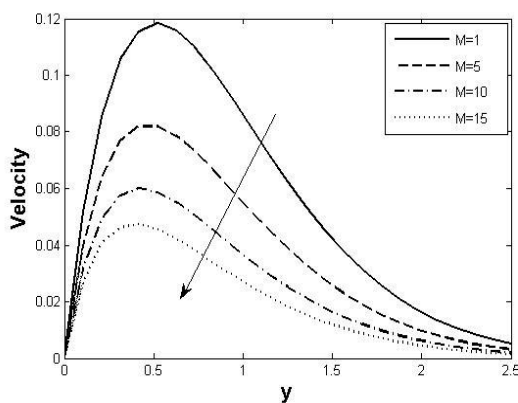


Fig. 2. Velocity against y for $M = 1, 5, 10,$ and 15 .

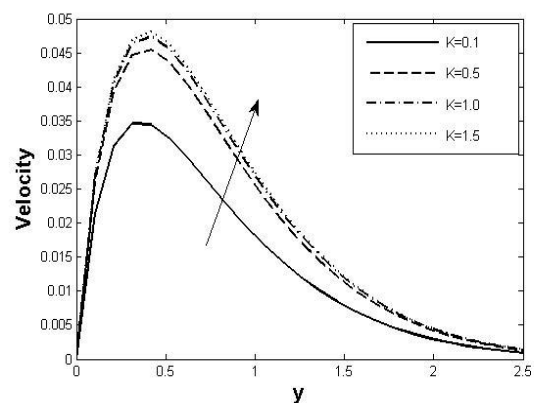


Fig. 3. Velocity against y for $K = 0.1, 0.5, 1,$ and 1.5 .

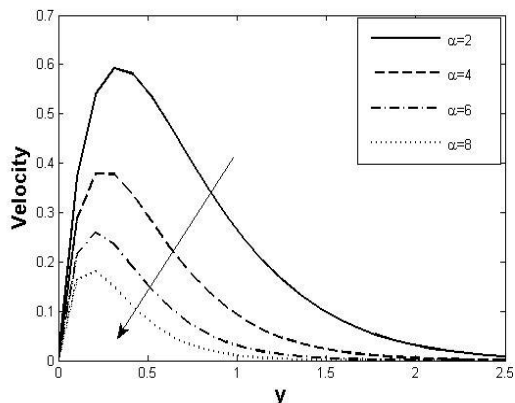


Fig. 4. Velocity against y for $\alpha = 2, 4, 6$ and 8 .

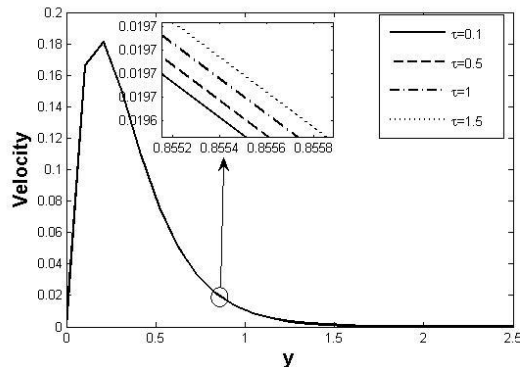


Fig. 5. Velocity against y for $\tau = 0.1, 0.5, 1,$ and 1.5 .

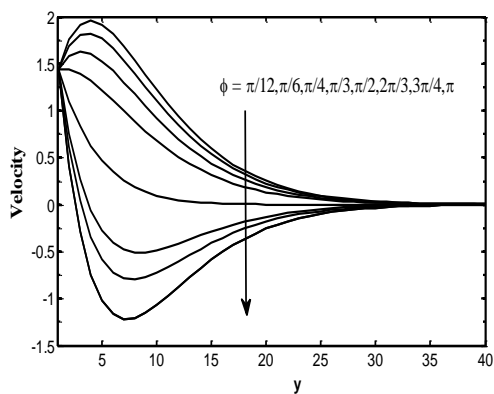


Fig. 6. Velocity against y for $\phi = \frac{\pi}{12}, \frac{\pi}{6}, \frac{\pi}{4}, \frac{\pi}{3}, \frac{2\pi}{3}, \frac{3\pi}{4}, \pi$

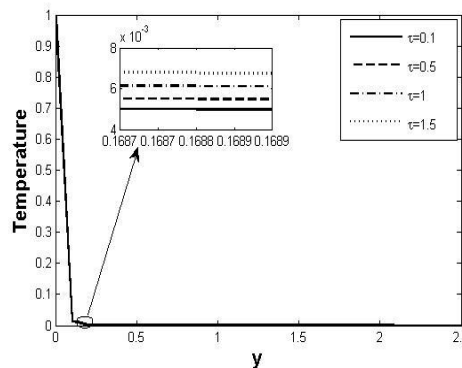


Fig. 7. Temperature against y for $\tau = 0.1, 0.5, 1,$ and 1.5 .

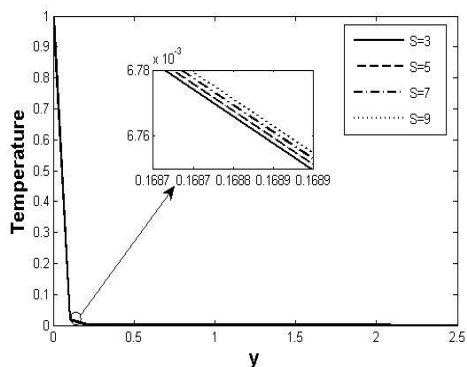


Fig. 8. Temperature against y for $s = 3, 5, 7,$ and 9 .

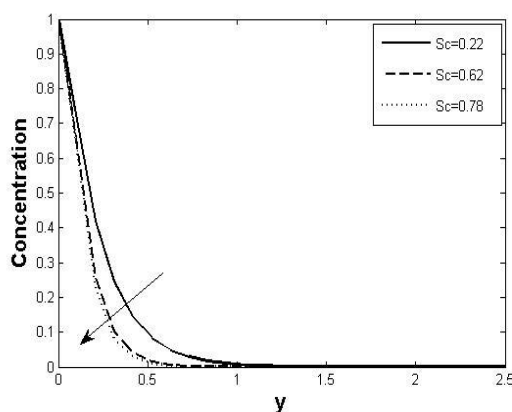


Fig. 9. Concentration against y for $Sc = 0.22, 0.62,$ and 0.78

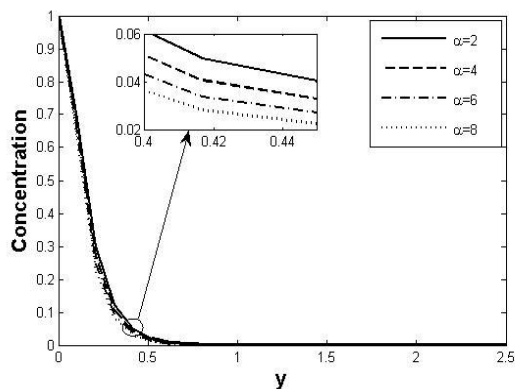


Fig. 10. Concentration against y for $\alpha = 2, 4, 6,$ and 8 .

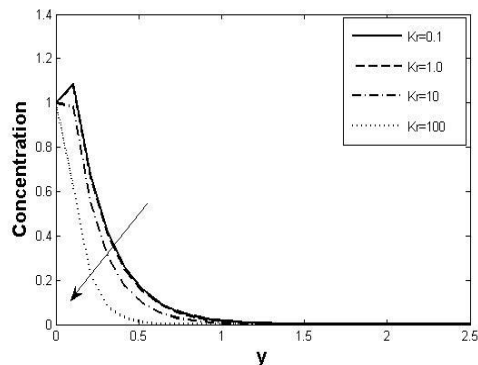


Fig. 11. Concentration against y for $Kr = 0.1, 1.0, 10,$ and 100 .

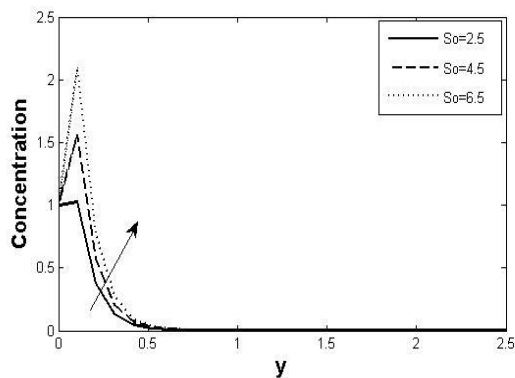


Fig. 12. Concentration against y for $So = 2.5, 4.5,$ and 6.5 .

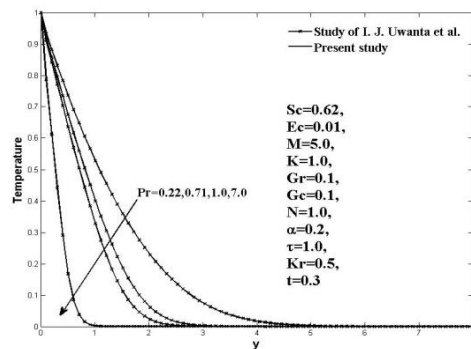


Fig. 13. Comparison of present results with that obtained by Uwanta et al. [14] with $b_1 = 0, So = 0, S = 0, b = 0$.

The influence of Kr on C is shown in Fig. 11. It is noticed from the figure, C is decrease whenever increasing the values of Kr . Because of the large values of Kr to decrease the thickness of the solutal boundary layer and raise the mass transfer of the fluid. The influence of So on C opposes the influence of chemical reaction Kr as shown in Fig. 12. Fig. 13 exhibits the validity of the outcomes compared with the fluid temperature for values of Pr . We equate the outcomes with the existing outcomes obtained by Uwanta et al. [14] by removing the inertia number, joule-heating parameter, heat source, and Soret parameters It shows that there is complete concurrence in their results.

Table 1 to table 3 presents the non-dimensional values of coefficient of Skin friction (Cf) and numbers of Nusselt (Nu) and Sherwood (Sh) for the numerical solution of governing equations. Table 1 displays the influence of non-dimensional parameters $Pr, \alpha, Gr, So, Sc, Kr, M, N, S$ and Gc on Cf . In table 1, it is observed that the augmenting values of Pr, Kr, M, N, Sc and α leads to a decline in Cf but for ascending values of Gr, Gc, S and So rises in Cf . Table 2 presents the influence of non-dimensional parameters Pr, Gr, N, b, α and So on Nu . From Table 2, observe Nu rises with increasing the values of Pr, N and α but increasing the values of Gr, b and So results fall of Nu . Similarly, table 3 exhibits the influence of non-dimensional parameters Sc, Kr, α and So on Sh . Results from table 3 show that Sh increases whenever the values of Sc, Kr and α increases but increasing So leads to a decrease of Sh .

Pr	Gr	Gc	Sc	Kr	α	M	N	S	So	Cf
0.71	1	1	0.62	0.1	1	1	0.1	1	1	0.7145
1										0.6811
	5									2.0936
	8									3.1401
		5								2.1216
		8								3.1231
			0.78							0.6967
			0.90							0.6857
				1						0.6871
				2						0.6617
					4					0.5248
					6					0.3742
						5				0.5340
						10				0.4143
							1			0.6898
							5			0.6305
								3		0.8042
								5		0.9927
									2.5	0.7927
									4.5	0.8957

Table 1. Coefficient of Skin friction

Pr	Gr	N	b	α	So	Nu
0.71	1	0.1	1	1	1	0.5522
1						0.8803
	5					0.4924
	8					0.4092
		1				0.9379
		5				1.9686
			10			0.4766
			50			0.1155
				4		1.8389
				6		2.6383
					2.5	0.5484
					4.5	0.5422

Table 2. Nusselt number

Sc	Kr	α	So	Sh
0.62	0.1	1	1	0.7722
0.78				0.8853
	1			1.0320

	2			1.2747
		4		1.1867
		6		1.5564
			2.5	0.4890
			4.5	0.1187

Table 3. Sherwood number

Conclusions:

The significant conclusions are made as follows

- Rising of angle of inclination leads to decrease the velocity.
- The influence of α and So on Nu is quite the opposite to that of the temperature θ of the fluid.
- The influence of Sc, α, Kr and So on Sh is quite the opposite to that of the concentration C of the fluid.

The effect of concentration C of the fluid rises with an increased Soret number So whereas reduces in Sherwood number Sh .

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