

# The Enhancing Influence of Process Parameters on Acrylonitrile Butadiene Styrene Composites Reinforced with Microcrystalline Cellulose

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## ABSTRACT

This study investigates the effects of different synthesis parameters of Acrylonitrile Butadiene Styrene/Microcrystalline Cellulose (ABS)/(MCC) composites on their physical, mechanical, and morphological properties. Composites were fabricated using a twin-screw extruder followed by hot pressing, with variations in the MCC volume fraction (0–8 vol%), screw speeds (10–20 rpm), and extrusion temperatures (150–170 °C). Density and flexural strength tests were conducted in accordance with ASTM standards, and the surface morphology was analyzed using Scanning Electron Microscopy (SEM). The results showed that incorporating 2–4 vol% of MCC improved both density and flexural strength by reducing voids and enhancing interfacial bonding. However, higher MCC contents led to particle agglomeration and diminished performance. A lower screw speed of 10 rpm facilitated better filler dispersion and stronger interfacial adhesion, yielding the highest flexural strength. Conversely, excessive screw speeds and elevated extrusion temperatures caused filler degradation, matrix shrinkage, and void formation, negatively impacting composite integrity. These findings demonstrate that careful optimization of filler content and processing parameters is essential to produce high-performance ABS/MCC composites with improved structural and mechanical characteristics.

*Keywords*-Acrylonitrile Butadiene Styrene (ABS); Microcrystalline Cellulose (MCC) filler; screw rotation speed; extrusion temperature; mechanical properties

## I. INTRODUCTION

ABS is a widely used engineering thermoplastic material in various applications, including the automotive industry, structural components, consumer goods, and household electronics [1, 2]. ABS is a copolymer composed of three main monomers: styrene, acrylonitrile, and butadiene, each contributing distinct characteristics to the overall material properties [3]. Styrene provides rigidity and ease of processing, acrylonitrile enhances the chemical resistance and mechanical strength, while butadiene adds superior impact resistance, making ABS highly suitable for applications requiring durability under dynamic loading [4-6]. This synergistic combination results in ABS exhibiting excellent mechanical properties and chemical resistance, making it ideal for engineering applications that demand both performance and durability [7]. In addition, ABS offers advantages, such as low density, ease of fabrication, and high precision mouldability, which further support its widespread use as an engineering polymer [8, 9]. To enhance the base polymer properties, ABS-based composites are often developed through the incorporation of reinforcing fillers [10-12].

MCC is one such filler commonly used to reinforce polymer matrices [13]. MCC consists of partially depolymerized natural cellulose or synthetic fibers, forming rod-like crystalline structures. These crystals are aggregates of cellulose microfibrils bonded via hydrogen interactions in a highly crystalline arrangement, while retaining some amorphous cellulose characteristics [14, 15]. MCC possesses high stiffness and exhibits strong interfacial adhesion with both fibers and polymer matrices, thereby improving the overall strength and stiffness of the composite [16, 17]. Significant improvements in the physical and mechanical properties of polymer composites reinforced with MCC have been demonstrated [18-24].

However, the final properties of polymer composites are strongly influenced by both their composition and manufacturing processes [25, 26]. It has been shown that the parameters of the manufacturing process, such as screw speed, barrel temperature, and die-end temperature during extrusion processing, can significantly affect the characteristics of the resulting composites [27-30]. For instance, higher extruder temperatures can enhance the material strength due to improved polymer melt flow and mixing [31, 32]. Likewise, increased screw speed promotes greater shear rates, leading to a more uniform and homogeneous filler dispersion within the matrix [33, 34].

While several studies have investigated ABS/MCC composites and explored various manufacturing aspects affecting their mechanical performance, research specifically focusing on the influence of extrusion processing parameters remains limited. Therefore, the present study aims to identify the optimal extrusion parameters to fabricate ABS/MCC composites with enhanced mechanical properties by investigating the effects of MCC volume fraction, extruder temperature, and screw speed on the mechanical performance of the composites.

## II. MATERIALS AND METHODS

### A. Materials

The ABS used in this study was LG Chem HI-121H, manufactured in Korea, with a melting point of 220 °C. The MCC powder had a particle size range of 20–160 μm, a melting point of 232 °C, and a density of 1.5 g/cm<sup>3</sup>.

### B. Synthesis

The fabrication of ABS/MCC composites was carried out while varying several parameters, as presented in Table I. A pre-treatment step was performed for both ABS and MCC. ABS granules were crushed using a mechanical crusher to a particle size smaller than 297 μm. MCC was dried in an electric oven at 100 °C for 6 h to reduce its moisture content. This drying process was used to minimize the thermal degradation of MCC during the composite pellet fabrication process [35]. The pre-treated ABS and MCC were then blended using a ball mill. The ABS/MCC composite pellets were, subsequently, produced using a twin-screw extruder, as depicted in Figure 1, and cut into lengths of 1–2 cm. Finally, the pellets were molded into ABS/MCC composites using a hot press machine at a pressure of 50 bar and a temperature of 160 °C for 30 min.

TABLE I. SPECIMEN VARIATIONS OF COMPOSITE ABS/MCC

| Sample code | ABS (vol%) | MCC (vol%) | Screw rotation (rpm) | Extruder temperature (°C) |
|-------------|------------|------------|----------------------|---------------------------|
| CM0         | 100        | 0          | 15                   | 160                       |
| CM2         | 98         | 2          | 15                   | 160                       |
| CM4         | 96         | 4          | 15                   | 160                       |
| CM6         | 94         | 6          | 15                   | 160                       |
| CM8         | 92         | 8          | 15                   | 160                       |
| CM4R10      | 96         | 4          | 10                   | 160                       |
| CM4R20      | 96         | 4          | 20                   | 160                       |
| CM4T15      | 96         | 4          | 15                   | 150                       |
| CM4T17      | 96         | 4          | 15                   | 170                       |



Fig. 1. Twin-screw extruder.

### C. Characterization

Characterization of the ABS/MCC composites was performed, including density measurements, flexural testing, and surface morphology observation. The density was measured in accordance with ASTM D3800 [36]. The flexural testing was performed based on ASTM D790 [37], using a universal testing machine equipped with a 50 kg load cell and a crosshead speed of 10 mm/min. The fracture surface morphology of the samples was examined deploying SEM.

### III. RESULTS AND DISCUSSION

Figure 2 presents the density values of the various ABS/MCC composites. The samples CM2 and CM4 exhibited increased densities compared to CM0 ( $1.032 \text{ g/cm}^3$ ), with values of  $1.065 \text{ g/cm}^3$  and  $1.069 \text{ g/cm}^3$ , respectively. This increase is attributed to the role of MCC as an effective filler that reduces the void content within the composite structure. MCC occupies microscopic gaps in the ABS matrix, thereby increasing the overall density [38]. However, increasing the screw rotation speed from 15 to 20 rpm (sample CM4R20) resulted in a reduced density of  $1.027 \text{ g/cm}^3$ . This phenomenon suggests that excessively high screw speeds shorten the residence time of the material inside the barrel, leading to incomplete mixing and non-uniform dispersion of MCC [39]. Consequently, MCC agglomeration and the formation of air voids occur, which decrease the composite's density. Additionally, the higher shear rate induced by increased screw speed can accelerate the degradation of the filler structure [40]. In contrast to the effect of screw speed, increasing the extrusion temperature from  $160 \text{ }^\circ\text{C}$  to  $170 \text{ }^\circ\text{C}$  (sample CM4T17) resulted in a slight decrease in density ( $1.061 \text{ g/cm}^3$ ). This outcome indicates that higher temperatures may lead to shrinkage due to a significant drop in the viscosity of ABS, which prevents the material from filling the mold completely [41].

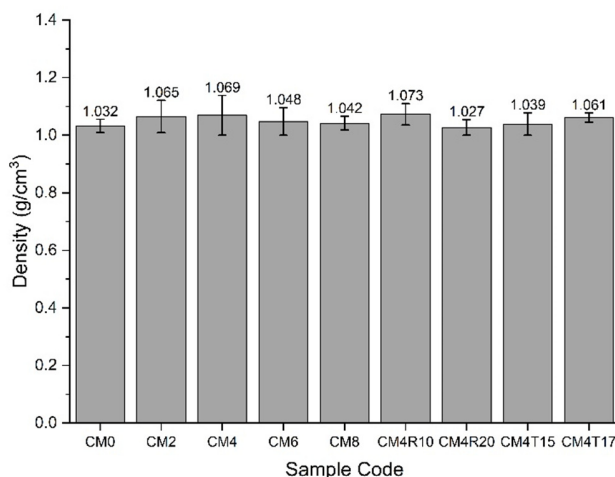


Fig. 2. Density of ABS/MCC composites.

The flexural strength of the ABS/MCC composites is presented in Figure 3. The results show that the addition of MCC at 2 vol% (sample CM2) and 4 vol% (sample CM4) led to an increase in flexural strength, reaching 54.91 MPa and 55.92 MPa, respectively, compared to the control sample CM0 (51.04 MPa). This improvement indicates that the incorporation of MCC in optimal amounts (2–4 vol%) enhances the flexural strength by reducing the voids and promoting a stronger interfacial bonding within the composite [42]. However, increasing the MCC content beyond 4 vol% resulted in a decline in flexural strength, as observed in samples CM6 and CM8. A decrease in flexural strength was also noted with increased screw rotation speed. The sample CM4R20, processed at a screw speed of 20 rpm, exhibited lower flexural strength of 50.02 MPa. This reduction is attributed to

insufficient residence time at higher screw speeds, leading to poor filler dispersion and inadequate bonding between MCC and the ABS matrix [43]. These weak interfacial regions act as stress concentrators and are prone to failure under bending loads [44, 45]. The effect of screw rotation speed was further confirmed by the CM4R10 sample, processed at 10 rpm, which exhibited the highest flexural strength of 57.08 MPa. The extrusion temperature also influenced the flexural strength of the ABS/MCC composites. The highest strength (55.92 MPa) was achieved at  $160 \text{ }^\circ\text{C}$  (sample CM4), which provides sufficient thermal energy to combine ABS with MCC without causing thermal degradation. In contrast, at  $170 \text{ }^\circ\text{C}$  (sample CM4T17), the flexural strength decreased to 53.24 MPa, indicating that the excessively low viscosity of ABS at higher temperatures may lead to shrinkage and the formation of internal voids within the extrudate [46]. The surface morphology of the ABS/MCC composites is shown in Figure 3.

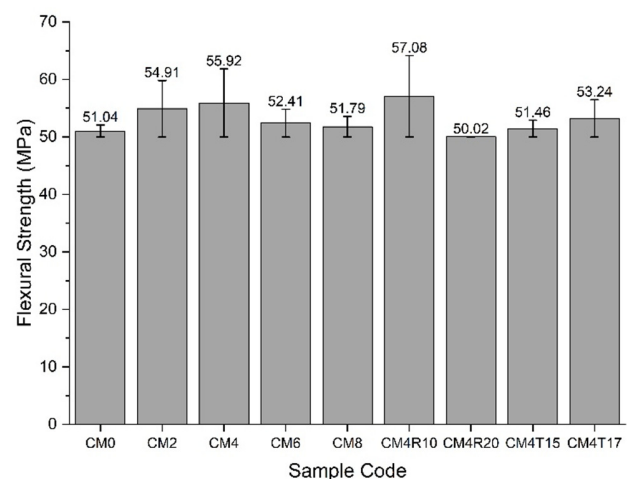


Fig. 3. Flexural strength of ABS/MCC composites.

For the CM0 sample, illustrated in Figure 3(a), the fracture surface appears relatively smooth and homogeneous. This observation is consistent with the composition of CM0, which contains no MCC filler, and therefore exhibits a morphology dominated by the pure ABS polymer matrix. The absence of filler particles results in a clean, non-porous surface structure. Such a morphology indicates that no filler distribution has occurred within the matrix, which corresponds to the lack of mechanical enhancement via void filling or particle reinforcement [47]. The distribution of MCC on sample CM8 is portrayed in Figure 3(b). In contrast to sample CM8, the fracture surface of sample CM4, evidenced in Figure 3(c), displays several regions, highlighted by circles that indicate the distribution of MCC particles within the ABS matrix. These observations suggest that the addition of 4 vol% MCC contributes to partial void filling within the matrix. This incomplete dispersion may result from an insufficient mixing time to achieve a homogeneous MCC distribution in the molten ABS. Additionally, the relatively high viscosity of ABS at the 15 rpm screw speed may not have provided adequate matrix wetting of the MCC particles.

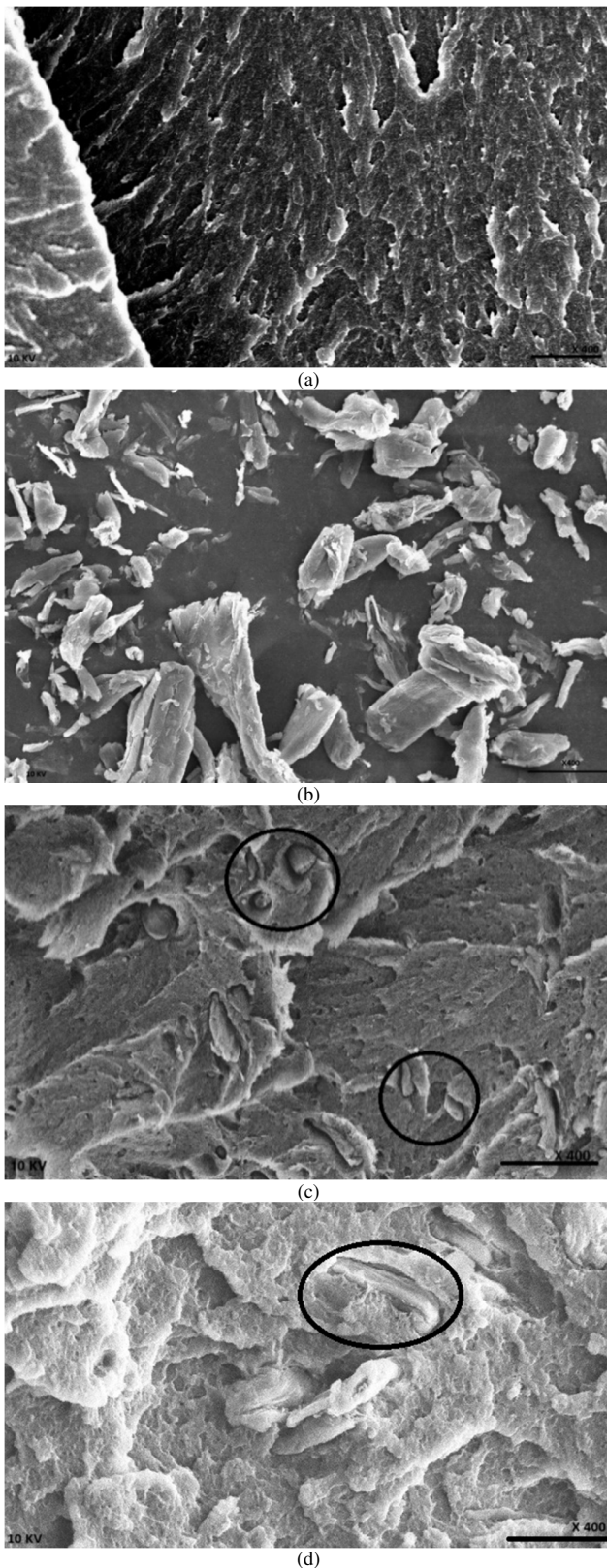


Fig. 4. Surface morphology of: (a) CM0, (b) CM8, (c) CM4, and (d) CM4R10.

The presence of voids and micro-gaps further indicates imperfect interfacial bonding, which could serve as initiation sites for microcracks when external loads are applied. This supports previous findings according to which, suboptimal mixing impedes interfacial interactions and reduces mechanical strength [48]. Sample CM4R10, which is shown in Figure 3(d), exhibits a denser and smoother fracture surface, with MCC particles well embedded in the ABS matrix, as indicated by the circled areas. In this case, the reduced screw speed of 10 rpm allows for longer residence time, facilitating a more thorough mixing. This results in a more uniform MCC distribution and stronger interfacial bonding between MCC and the ABS matrix. The observed phenomena of fiber pullout and fiber breakage suggest that some MCC particles bonded strongly enough with the matrix to fracture under mechanical loading. The fiber breakage indicates a robust interfacial adhesion, while the fiber pullout reflects areas where MCC was not fully integrated with the matrix [48]. These findings highlight that processing parameters, particularly screw speed, play a critical role in optimizing interfacial bonding and improving the flexural strength of ABS/MCC composites.

#### IV. CONCLUSION

This study investigated the effects of MCC volume fraction, screw rotation speed, and extrusion temperature on the mechanical and morphological properties of Acrylonitrile Butadiene Styrene/Microcrystalline Cellulose (ABS)/(MCC) composites. Adding 2–4 vol% MCC enhanced the density and flexural strength by improving filler dispersion and interfacial bonding. In contrast, contents above 4 vol% caused agglomeration of the MCC and voids, reducing performance. A screw speed of 10 rpm improved mixing and residence time, yielding better mechanical strength and uniform morphology, while the 20 rpm speed decreased dispersion quality and damaged the filler. The optimal extrusion temperature was 160 °C. A higher temperature (170 °C) reduced strength due to lower viscosity and shrinkage. Unlike prior studies focusing only on MCC content, this work evaluates the combined effects of filler content and processing parameters. The integrated approach clarifies processing–structure–property relationships in ABS/MCC systems. These findings highlight the value of process optimization for high-performance, bio-based thermoplastic composites.

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