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# Experimental Study of Transducer Harmonics Effect on Pump Unit Energy Consumption

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Frequency control techniques have been widely applied in chemical processing. However the effects on whole unit energy consumption caused by transducer high harmonics and its additional loss have not been paid enough attention. An experimental study was conducted by using self-priming pump unit as a research object, utilizing NI virtual instrument, and Labview test software and high-frequency electric parameter analyzer. Performance parameters of the pumps and electric parameters of pump system were measured before and after pump unit filtering. Pump unit energy consumption under both circumstances was computed and analyzed. It can be found that unit energy consumption differs from 3% to 6%, while electric motor efficiency differs in 10 percentage points. Pump unit energy consumption difference increases with the loss of frequency before and after filtering. All the above has provided a basis for proper use of transducers and determining the speed range of the pump unit.

## 1. Introduction

A Pump unit is the main equipment and major energy consumer in a chemical process. With the development of energy conservation and pollution reduction, frequency change and speed adjusting has been increasingly used for saving which was confirmed by Chen (2002) and Luo (2015). However, Chen (2003) et al reported that voltage waveform and current waveform of incoming power will distort because of the high-frequency harmonics created by the variable current loop of transducer input section. The increasing copper and iron loss and mechanical vibration of the pump unit caused by harmonics of motors will result in increase of the whole pump unit system energy consumption and the instability of control system. In the transducer-motor system, it is excessive harmonic currents that lead to the increase of motor heating quantity, reduction of motors lifetime and insulation breakdown of motors, or more seriously cable burst which was confirmed by Francisco (2006) et al.

This paper has adopted NI virtual instrument, Labview test software and a high-frequency electric parameter analyzer to analyze and compare performance parameters of pumps and electric parameters before and after pump unit filtering as well as the effect caused by speed range on the whole pump unit energy consumption

## 2. Components of transducer harducer harmonics

Usually transducers utilize abundant nonlinear power electronic components such as thyristors. The way transducers absorb energy from the power grid is not a successive sine-wave, but by obtaining current from power grid by pulsation intermittent mode. Such pulsation current and on-way impedance together form pulsation voltage drop superimposing on the voltage of the power grid, which make the voltage distort. According to Fourier analysis, such nonperiodic sine-wave current consists of harmonics whose frequency is not lower than the fundamental wave. Thus, the equations are as follow according to Fuchs (2004).

$$\begin{cases} u_{as} = U_{1m} \sin \omega t + U_{5m} \sin 5\omega t + U_{7m} \sin 7\omega t + \dots \\ u_{bs} = U_{1m} \sin (\omega t - 120^{\circ}) + U_{5m} \sin (5\omega t + 120^{\circ}) + U_{7m} \sin (7\omega t - 120^{\circ}) + \dots \\ u_{cs} = U_{1m} \sin (\omega t + 120^{\circ}) + U_{5m} \sin (5\omega t - 120^{\circ}) + U_{7m} \sin (7\omega t + 120^{\circ}) \dots \end{cases}$$
(1)

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In the equations,  $u_{as,n}$ ,  $u_{cs}$  are three-phase voltage instantaneous values.  $U_{1m}$ , are voltage values of the first, fifth and seventh harmonics. From the first equation it can be found that there are no integral harmonics in the voltage instantaneous values. Harmonics of transducers mainly consist of the 5th, 7th, 11th, 13th, 17th, 19th harmonics with no multiple of 3nd harmonics because the three angles of the different phases have 120° difference.

#### 3. Effects of harmonics on the pump units

#### 3.1 Effects of harmonics on the motors

The motor is an important part of pump units. Alternating-current with harmonics will make the performance of motors different from the one supplied by sine-wave power because the frequency power outputs the fundamental as well as the harmonic voltage and current.

High frequency harmonics selected from the stator current will increase stator copper loss. But skin effect resulting from the high-frequency current in the rotor multiplies loss of rotor resistance many times and increases copper loss of rotor resistance. Thus, magnetic and electric load increases while power and power factor decreases when harmonic voltage supplies the asynchronous motor with power which was confirmed by Fuchs (2004) and Carbone (2001).

Harmonic effect can also result in motor ripple in the torque, which generates vibration, noise, makes the pump unit system unstable and finally influences the work of the control system.

Variable frequency drive in the pump unit creates efficiency loss in itself and will increase the temperature of the winding if it generates harmonics in the motor winding which accelerates the damage of motor insulation winding under excessively high temperature for long times.

#### 3.2 Effects of harmonics on the pump unit energy consumption

The equation below can be utilized when quantitatively evaluating N, called pump unit energy consumption according to Tang (2007).

$$N = \frac{\rho g H Q}{367 \eta_{\rm P} \eta_{\rm m} \eta_{\rm v}} \tag{2}$$

In equation, *H*-total head, m; *Q*-flow, m<sup>3</sup>/h;  $\eta_p$ -pump efficiency, %;  $\eta_m$ -motor efficiency, %;  $\eta_v$ —transducer efficiency, %.

From the Equ (1) it can be revealed that motor efficiency has influence on the energy consumption of pump units and will decrease because of power and power factor of the motor, which will increase energy consumption of the whole pump unit which was also confirmed by Liu (2006). Also because the calculation formula of motor efficiency is:

$$\eta_{\rm m} = P_{\rm out} / P_{\rm in} \tag{3}$$

(4)

$$P_{\rm out} = T^* n/9550$$

*T*-torque, N·m; *n*-rotating speed, r/min;  $P_{out}$ -output power of motor, kW;  $P_{in}$ -input power of motor, Kw. The efficiency of transducer can be regarded as 1 because it is high. Equation 3 and 4 above can be substituted into Equ (2) to get

$$N = \frac{9550P_{\rm in}\rho gHQ}{367Tn\eta_{\rm v}} \tag{5}$$

#### 4. Experiment

During the experiment, performance parameters of the pumps and electric parameters of the pump system can be measured and energy consumption of the pump unit before and after filtering can be analyzed and compared through frequency adjustment by transducer so as to change the rotating speed. Simplified physical model of experiment device is shown in the illustration. The experimental equipment are shown in the Table 1.

974



Figure 1: A simplified physic model of the simplified experiment of pump-units system

| Equipment  | Parameter  |
|--|--|
| Self-priming pump  | Q=15 m³/h; <i>H</i> =35 m; <i>n</i> =2600 r/min;   |
| Transducer<br>Three-phase asynchronous motor<br>Torque and speed sensors | Mitsubishi FR-F740<br><i>U</i> 1N=380 V; <i>P</i> 1N=4.0 kW<br>Rated load torque 100 N⋅m; accuracy level 0.2 |
| Pressure transmitter   | WT1151GP, accuracy $\pm 0.25\%$ , head $\pm 100$ kP <sub>a</sub> ; accuracy level 0.2                        |
| Flowmeter<br>Electric parameter analyzer                                 | Turbine flowmeter, accuracy ±0.5%,<br>Qingzhi8962C1  |

#### 4.1 Comparison of electric parameter waveforms before and after filtering

A RLC sin-wave filter according to Ji (2006) and Su (2003) was chosen for the filtering with the Bode plot as shown in Fig 2.



Figure 2: Bode plot of the filter

In the Fig 3 output voltage waveforms of the transducer at 50Hz frequency before and after filtering are compared through the high-frequency electric parameter analyzer. It can be found in the figure that direct output voltage waveforms of the transducer before filtering is not the standard sine-wave but the after one is standard in that intersection point of SPWM waves and triangular carrier generates output voltage and current. It can be analyzed that such voltage waveforms include comparatively high-frequency harmonics through resolving of the Fourier series in the Equ (1).



Figure 3: A comparison of oscillogram for the frequency converter filtering pre and post under the 50 Hz

#### 4.2 Comparison of pump unit energy consumption before and after filtering

During the experiment of frequency change and speed adjusting energy consumption of the pump unit, the flow of the pump should be at rated flow of 15 m<sup>3</sup>/h through adjusting the valve under condition of power frequency. Then adjust the transducer, adjust the rotating speed by changing frequency so as to change performance parameters of pump unit as well as electric parameters of pump system. Performance parameters of the pump in the pump unit can be measured under different frequency as is shown in Table 2. Energy consumption of the pump unit can be calculated before and after filtering through Equation 5 as is shown in the Table 3 and 4.

Table 2: The performance parameters of self-priming centrifugal pump

| Frequency<br>(Hz) | Flow (m <sup>3</sup> /h) | Torque (N·m) | Rotating speed (r/min) | Total head (m) | Pump efficiency<br>(%) |
|-------------------|--------------------------|--------------|------------------------|----------------|------------------------|
| 50                | 15.09                    | 12.89        | 2915.19                | 37.77          | 40.28                  |
| 45                | 13.55                    | 10.43        | 2618.21                | 30.49          | 40.11                  |
| 40                | 11.97                    | 8.36         | 2310.4                 | 23.92          | 39.38                  |
| 35                | 10.41                    | 6.63         | 2020.16                | 18.11          | 37.35                  |
| 30                | 8.77                     | 4.84         | 1713.11                | 12.93          | 36.28                  |
| 25                | 7.14                     | 3.46         | 1419.34                | 8.68           | 33.51                  |

| Table 3: Electric | parameters and | d enerav consun | nption before | ə filterina |
|-------------------|----------------|-----------------|---------------|-------------|
|                   |                |                 |               |             |

| Frequency | Input power of motor | Output power of motor | Efficiency of motor | Energy           |
|-----------|----------------------|-----------------------|---------------------|------------------|
| (Hz)      | (kW)                 | (kW)                  | (%)                 | consumption (kW) |
| 50        | 4.481                | 3.935                 | 87.82               | 4.321            |
| 45        | 3.306                | 2.862                 | 86.57               | 4.4              |
| 40        | 2.395                | 2.021                 | 84.42               | 4.639            |
| 35        | 1.66                 | 1.402                 | 84.48               | 4.81             |
| 30        | 1.085                | 0.868                 | 80.08               | 5.155            |
| 25        | 0.674                | 0.513                 | 76.11               | 5.339            |

Table 4: Electric parameters and energy consumption after filtering

| Frequency | Input power of motor | Output power of motor | Efficiency of motor | Energy consumption |
|-----------|----------------------|-----------------------|---------------------|--------------------|
| (Hz)      | (kW)                 | (kW)                  | (%)                 | (kW)               |
| 50        | 4.354                | 3.938                 | 90.44               | 4.207              |
| 45        | 3.179                | 2.808                 | 88.32               | 4.270              |
| 40        | 2.246                | 2.064                 | 91.88               | 4.268              |
| 35        | 1.534                | 1.377                 | 89.76               | 4.455              |
| 30        | 0.979                | 0.890                 | 90.91               | 4.656              |
| 25        | 0.571                | 0.489                 | 85.79               | 4.758              |

Two curves of energy consumption before and after filtering are shown in the Figure 4. With the reduction of frequency, the increasing difference of energy consumption between before and after filtering is approximately 3%~6%.



Figure 4: Energy consumption of the pump-units system before and after filtering



Figure 5: Motor efficiency of the pump-units system before and after filtering

The curves of motor efficiency before and after filtering are shown in the Figure 5. From the figure it can be found that with the reduction of frequency the motor efficiency decreases before and after filtering. Also, motor efficiency differs greater when frequency and rotating speed decrease. That is, the effect of harmonic motor efficiency increases in the low frequency range. Efficiency of the harmonic motor before and after filtering differs in 10 percent when the frequency decreases to 25 Hz. Therefore, filters or reactors should be utilized to cut down the effect of harmonics when using transducers to change the speed of pump unit.

#### 5. Conclusions

1) The effect of transducer harmonics on pump unit energy consumption is studied through experiment, during which the difference of energy consumption between before and after filtering is compared which is about 3%~6%. The motor efficiency differs by 10 percent.

2) Transducers can be utilized to change the speed of a pump. When the rotating speed is high, filters can be chosen. Only one water pump is utilized during the experiment in this paper, which is of reference value for other pump units.

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