

VOL. 43, 2015





DOI: 10.3303/CET1543307

Vapour-Liquid Equilibrium Prediction of Carbon Dioxide in an Aqueous Alkanolamine Solution Using Deterministic and Stochastic Algorithms

Djaballah Mohamed Larbia, Kabouche Azeddine*,b

^aEcole polytechnique, Université Constantine 3, Algeria

^bDépartement GP, Laboratoire de Chimie Appliquée et Technologie des Matériaux, Université d'oum El Bouaghi, Algeria kabouche66@yahoo.fr

Carbon dioxide capture by reactive absorption with aqueous alkanolamines has a great importance in reducing CO₂ emissions. The development or the choice of thermodynamic models for (CO₂ + H₂O + alkanolamine) systems presents some specific difficulties. In this work PITZER model have used to correlate and predict the vapour-liquid equilibrium of CO₂ in aqueous monoethanolamine (MEA) solutions, interaction parameters were calculated by using simplex (deterministic algorithm) and genetic algorithms (stochastic algorithm). The solubility of CO₂ in aqueous solutions of 15, 30, 45 and 60 mass % of MEA has been considered over several temperatures and CO₂ partial pressures. The predicted results of vapour-liquid phase equilibrium have been found to be in good agreement with the experimental measurements.

1. Introduction

CO₂ capture by absorption with aqueous alkanolamines solutions is considered as an important technology to reduce CO₂ emissions from fossil-fuel-fired power plants and to help alleviate global climate change (Zhang et al., 2009). Chemical absorption of CO₂ can be used in post-combustion (Athanasios et al., 2014). Kinetic studies of CO₂ by chemical absorption (Molina and Bouallou, 2013) are a key step to give rigorous expression of several parameters that one can cite the very important equilibrium constant. The development of thermodynamic models for (CO₂ + H₂O + alkanolamine) systems is quite complex. The more rigorous models that take into account non-ideality are based on a system of equations for chemical equilibria (Kabouche et al., 2005), phase equilibria, charge, and mass balances. In this work, the fugacity coefficients ϕ were obtained from a truncated virial equation of state and the activity coefficients γ calculated using a Pitzer model in order to correlate and predict the vapour-liquid equilibrium of the (CO₂+H₂O+MEA) system. The required equilibrium constant for chemical reactions were obtained from literature. Two different literature sources giving correlations of the equilibrium constant (as function of temperature) of deprotonation of MEA, hydration of CO₂ and dissociation of carbamate were used in this work to adjust the model cited above.

2. Modelling of phase equilibria

When considering dissolution of CO_2 in aqueous MEA solution, chemical reactions (1) to (5) may take place in the liquid phase:

$MEAH^+ \stackrel{K_1}{\leftrightarrow} MEA + H^+$	(1)
$CO_2 + H_2O \stackrel{K_2}{\leftrightarrow} H^+ + HCO_3^-$	(2)
$HCO_3^- \stackrel{K_3}{\leftrightarrow} H^+ + CO_3^{2-}$	(3)
$MEACOO^{-} + H_2O \stackrel{K_4}{\leftrightarrow} MEA + HCO_3^{-}$	(4)
$H_2O \stackrel{K_5}{\leftrightarrow} H^+ + OH^-$	(5)

Please cite this article as: Djaballah M.L., Kabouche A., 2015, Vapor-liquid equilibrium prediction of carbon dioxide in an aqueous alkanolamine solution using deterministic and stochastic algorithms, Chemical Engineering Transactions, 43, 1837-1842 DOI: 10.3303/CET1543307

Usually the Henry's law and the equilibrium reaction constants are considered as a function of temperature. The general dependency of these constants to temperature is given by the following equation:

$$\ln(K_N \text{ or } H) = \frac{a}{T} + b \cdot \ln T + c \cdot T + d, \quad N = 1 \text{ to } 5$$
(6)

The corresponding coefficients for reactions (1) to (5) are summarized in table (1). The molality scale values of the coefficients are given in this Table (1).

Reaction	а	b	С	d	°K	literature
1	-17.3	0	0.05764	-38.846	293-353	(Hamborg and Versteeg,2009)
2	-12092.1	-36.7816	0	235.482	273-498	(Edwards et al,1978)
3	-12431.7	-35.4819	0	220.067	273-498	(Edwards et al,1978)
4	-1545.3	0	0	2.151	293-323	(Aroua et al,1999)
5	-13445.9	-22.4773	0	140.932	273-498	(Edwards et al,1978)
H_{CO_2}	-9624.4	-28.749	0.01441	192.876	273-473	(Rumpf and Maurer, 1993)

Table 1: Coefficients of Eq(6) for the equilibrium constant K_N

Another alternative to calculate the equilibrium constants using the parameters of Table 2 is given by the following equation:

$$ln (K_N \text{ or } H) = a + \frac{b}{T} + c. ln T + d. T + e/T^2$$

Table 2: Coefficients of equation (7) for the equilibrium constant K_N

Reaction	а	b	С	d	е	°K	literature
1	- 1.73782	- 6092.85	0	0.001157	0	273 - 398	(Hasse et al ,2013)
2	-1,203.01	68,359.6	188.444	- 0.206424	- 4,712,910	273 - 673	(Patterson et al, 1982)
4	- 5.9680	2888.6	0	0	0	293 - 333	(McCann,2012)

3. Thermodynamic Framework

In $(CO_2 - MEA - H_2O)$ system, the existence of neutral specie pure alkanolamine MEA and H₂O, and ionic species – protoned alkanolamine, HCO₃⁻ and carbamate ion MEACOO⁻ in the equilibrated liquid phase have been considered. For simplicity, the free molecular species CO₂ and the ionic species CO₃⁻² and OH⁻ in the liquid phase have been neglected since concentration of these species are very low compared to the other species present in the equilibrated liquid phase. Several previous workers, one can cite (Posey, 1996), have observed that neglecting the concentration of free molecular CO₂, and OH⁻ and CO₃⁻² ions in the liquid phase in this system for CO₂ loading below 1.0 does not result in significant error in the VLE predictions. It is thus assumed that almost all of the dissolved CO₂ is converted into HCO₃⁻ ions. It is also assumed a physical solubility (Henry's law) relation for the (noncondensible) acid gases and a vapour pressure relation for water. (if the system contains other volatile species, such as hydrocarbons, these can be accounted by additional isofugacity relations based, for example, on Henry's law for sparingly soluble components, or on vapour pressures for condensibles). Thus, the following relation is applied: $\phi_{CO_2} \cdot \gamma_{CO_2} \cdot P = H_{CO_2} \cdot \gamma_{CO_2} \cdot m_{CO_2}$ (8)

Where ϕ_{CO_2} is the fugacity coefficient of CO_2 , y_{CO_2} is mole fraction, H_{CO_2} is a Henry's constant for the acid gas in pure water, *P* is the total pressure. The partial pressure of carbon dioxide is calculated by the following relation (Mondal, 2009):

$$P_{CO_2} = \frac{H_{CO_2}}{\phi_{CO_2}} \cdot \frac{K_1 K_4}{K_2} \cdot \frac{\gamma_{MEAH^+} m_{MEAH^+} \gamma_{MEACOO^-} m_{MEACOO^-}}{(\gamma_{MEA} m_{MEA})^2}$$
(9)

1838

(7)

4. Activity coefficient model

Activity coefficients γ_i of ionic and molecular species i present in solution are calculated using the Pitzer equation as modified by (Edwards et al., 1978).

$$\ln \gamma_{i} = -A_{\phi} z_{i}^{2} \left(\frac{\sqrt{I}}{1+1.2\sqrt{I}} + \frac{2}{1.2} \ln(1+1.2\sqrt{I}) \right) + 2 \sum_{j \neq w} m_{j} \left(\beta_{ij}^{0} + \frac{\beta_{ij}^{1}}{2I} [1 - (1+2\sqrt{I})exp(-2\sqrt{I})] \right) - z_{i}^{2} \sum_{j \neq w} \sum_{k \neq w} m_{j} m_{k} \frac{\beta_{jk}^{1}}{4I^{2}} [1 - (1+2\sqrt{I}+2I)exp(-2\sqrt{I})]$$
(10)

Where *I* is ionic strength of the solution, z_i and m_i are charge and molality of species *i*. A_{ϕ} is Debye-Huckel limiting slope of osmotic coefficient and β_{ij}^0 and β_{ij}^1 are interaction parameters. A_{ϕ} is calculated using equation (11) proposed by (Chen et al,1982):

$$A_{\phi} = -61.44534 \exp\left(\frac{T - 273.15}{273.15}\right) + 2.864468 \exp\left[\frac{T - 273.15}{273.15}\right]^{2} + 183.5379 \ln\left(\frac{T}{273.15}\right) \\ - 0.6820223(T - 273.15) + 7.87595.10^{-4}(T^{2} - 273.15^{2}) \\ + 58.95788\left(\frac{273.15}{T}\right)$$
(11)

Activity of water is derived from equation (10) using the Gibbs-Duhem equation:

$$\ln a_{w} = \frac{M_{w}}{1000} \left(\frac{2A_{\phi}I^{1.5}}{1 + 1.2\sqrt{I}} - \sum_{i \neq w} \sum_{j \neq w} m_{i}m_{j}[\beta_{ij}^{0} + \beta_{ij}^{1}exp(-2\sqrt{I})] - \sum_{i \neq w} m_{i} \right)$$
(12)

Where M_w is molecular weight of water.

5. Data regression

In this work, the solubility data of CO_2 in aqueous alkanolamine solutions of various concentrations, in a wide range of CO_2 partial pressure and temperatures and below a CO_2 loading of 1.0 mol CO_2 /mol amine, have been used to estimate the interaction parameters by regression analysis. The data reported by (Aronu et al, 2011) were used to extend the range of application of the model.

The data regressions were carried out at 313 K and 333 K. The objective function (OF) used for optimization is given by:

$$OF = \sum \left| \frac{\left\{ \left(P_{CO_2} \right)_{cal} - \left(P_{CO_2} \right)_{exp} \right\} \right|}{\left(P_{CO_2} \right)_{exp}} \right|$$
(13)

We investigate the numerical values of interaction parameters that will minimize (OF) the difference between the measured values of equilibrium partial pressure of CO₂ over alkanolamine solutions and the values calculated from the model. The objective function chosen in this work takes care of giving uniform weightage throughout the entire range of partial pressure.

The objective function has been optimized by the unconstrained nonlinear minimization Nelder-Mead Simplex method (NMS) and Genetic algorithm (GA) (Kabouche et al., 2012).

6. Results and discussions

Interaction parameters $\beta_{i,j}^0$ and $\beta_{i,j}^1$ are adjusted with experimental data (points) using two different model (Eq. 6 and 7) from the literature to calculate K_1 , K_2 and K_4 correlations cited above. Two different kinds of optimization techniques; Deterministic (NMS) and Genetic algorithm (GA) have been used for predicting phase equilibria. For the $(CO_2 - MEA - H_2O)$ system, the interaction parameters were determined using solutions of 15, 30, 45 and 60 mass % of MEA at 313 K and 333 K. The literature data has been taken from (Aronu et al., 2011) and model of Eq (9) was used. The equilibrium constants were calculated using two different formula (6) and (7), a discrepancy can be noted in the figures between the curve in solid lines (model of Eq(7)) and the curve in dashed lines (model of Eq(6)), the best results were obtained for the curve in solid lines in figure 1 to 4 using NMS algorithm and figure 8 to 10 using GA algorithm for the temperature 313 K however the results in figures 5 and 6 for temperature 333 K using NMS algorithm and in Figures 7 and 12 for temperature 333 using GA algorithm shows that the model in dashed lines gives the best results. In general the two algorithms give good results using the model of Eq(7) rather than of Eq(6).



Figure1NMS method %MEA=15, T=313 K



Figure 3: NMS method %MEA = 45, T = 313 K



Figure 5: NMS method %MEA = 15, T = 333 K



Figure 2 NMS method % MEA=30, T=313 K



Figure 4: NMS method % MEA = 60, T = 313 K



Figure 6: NMS method % MEA = 30, T = 333 K



Figure 7: GA method %MEA = 15, T = 313 K



Figure 9: GA method %MEA = 45, T = 313 K





Figure 10: GA method % MEA = 60, T = 313 K

201



(R d y) 10 5 0.05 0.1 0.15 0.2 0.25 0.3 0.35 0.4 0.45 0.5 CO₂ Loading

Figure 11: GA method %MEA = 15, T = 333 K

Figure 12: GA method % MEA = 30, T = 333 K

7. Conclusion

In this work, a thermodynamic model was used to correlate solubility data (Aronu et al, 2011) considering the effect of MEA deprotonation, hydration of CO_2 and dissociation of carbamate equilibrium constants. The thermodynamic model is based on PITZER equations from Eq(10) to Eq(12). The model was applied to molecular and ionic species generated by the equilibrium reactions of equations A to E for calculating activity coefficients after regression of solubility data (using optimization methods). The fugacity coefficient is calculated using the virial equations. Finally, in this work, two models for calculating the equilibrium constants were considered; in general the results show that the model in Eq(7) gives the best results. As stochastic algorithm, the genetic algorithm (GA) is used and as deterministic model, the Nelder-Mead Simplex (NMS) method is used. The two optimization models used in this work give a quite good approximations to the experimental data for system ($CO_2 + H_2O +$ alkanolamine) at 313 K and 333 K considering the solubility of CO_2 in aqueous solutions of 15, 30, 45 and 60 mass % of MEA.

Reference

- Aronu U. E., Gondal S., Hessen E T., Haug-Warberg T., Hartono Ardi., Hoff K A., Svendsen H F., 2011, Solubility of CO₂ in 15, 30, 45, and 60 mass% MEA from 40 to 120 °C and model representation using extended UNIQUAC framework. Chem. Eng. Sci. 66, 6393-6406.
- Aroua M. K., Benamor A., Haji-Sulaiman M. Z., 1999, Equilibrium constant for carbamate formation from monoethanolamine and its relationchip with temperature, J. Chem. Eng. Data. 44, 887-891.
- Chen C. C., Britt H. I., Boston J. F., Evans L. B., 1982, Local compositions Model for Excess Gibbs Energy Electrolyte systems Part: Single Solvent, Single completely Dissociated Electrolytes Systems, AICHE J. 28, 588-596
- Edwards T. J., Maurer G., Newman J., Prausnitz J. M., 1978, Vapour-liquid equilibria in multicomponent aqueous solutions of volatile weak electrolytes, AICHE J. 24, 966-976
- Hamborg E. S., Versteeg G. F., 2009 Dissociation constants and thermodynamic properties of amines and alkanolamines from 293 to 353 K. J. Chem. Eng. Data. 54, 1318-1328
- Hasse, H., Wagner, M., Harbou, I., Kim, J., Ermatchkova, I., 2013, Solubility of carbon Dioxide in Aqueous Solutions of Monoethanolamine in the Low and High Gas Loading Regions, J. Chem. Eng. Data., 58, 883-895
- Kabouche A., Meniai A.H., Bencheikh-lehocine M. A., 2005, Modeling The Absorption of Acidic Gases by Alcanolamine Solutions Incorporating Several Reactions, Chemical Engineering Technology, 28, 67–71.
- Kabouche, A., Boultif, A., Abidi, A., Gherraf, N, 2012, Interaction parameter estimation in liquid-liquid phase equilibrium modeling using stochastic and hybrid algorithms, Fluid Phase Equilibria, 336,113–121.
- McCann. N., 2012, Personal communication.
- Molina C. T., Bouallou C., 2013, Kinetics Study and Simulation of CO₂ Absorption into Mixed Aqueous Solutions of Methyldiethanolamine and Diethanolamine. Chemical Engineering Transactions, 36, 319-324.
- Mondal Kumar, T., 2009, Phase Equilibrium Modeling in Gas Purification System, Dissertation of Master of Technology, Chemical Engineering Department, National Institute of Technology, India.
- Papadopoulos A.I., Badr S., Chremos A., Forte E., Zarogiannis T., Seferlis P., Papadokonstantakis S., Adjiman C.S., Galindo A., Jackson G.,2014, Efficient Screening and Selection of Post-Combustion CO₂ Capture Solvents. Chemical Engineering Transactions, 39, 211-216. Patterson C., Slocum G., Busey R., Mesmer R., 1982, Carbonate equilibria in hydrothermal systems: First ionization of carbonic acid in NaCl media to 300 °C. Geochim. Cosmochim. Acta., 46, 1653-1663.
- Posey, M. L, 1996, Thermodynamic model for acid gas loaded aqueous alkanolamine solutions, PhD Thesis, University of Texas, Austin, USA.
- Rumpf B., Maurer G., 1993, An experimental and theorical investigation on the solubility of carbon dioxide in aqueous solutions of strong electrolytes, Ber. Bunsen. Phys. Chem., 97, 85-97.
- Zhang Y., Chen H., Chen C. C., Plaza J. M., Dugas R., Rochelle G. T., 2009, Rate-Based Process Modelling Study of CO₂ Capture with Aqueous Monoethanolamine Solution. Ind. Eng. Chem. Res., 48, 9233–9246.