

## Carbon Dioxide Absorption into Mixed Amines in a Cross-Flow Rotating Packed Bed

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This study investigates the feasibility of applying a cross-flow rotating packed bed (RPB) to absorb carbon dioxide (CO<sub>2</sub>) by mixed amine solutions from gaseous streams. The cross-flow RPB has an inner radius of 2.4 cm, an outer radius of 4.4 cm and an axial height of 12.0 cm. Wire mesh was used as packings. Rotor speeds ranged from 600 to 1800 rpm, providing 14~123 equivalent gravitational force. The removal efficiency of CO<sub>2</sub> was determined at various values of operating parameters, including the rotor speed, gas flow rate, mixed amine flow rate, and absorbent type. Our experimental results demonstrated that the removal efficiency of CO<sub>2</sub> increased with the rotor speed and mixed amine flow rate, however, decreased with the gas flow rate. Furthermore, CO<sub>2</sub> removal efficiency using PZ/MEA was superior to those using MEA and AMP/MEA. Consequently, PZ/MEA could be used in a cross-flow RPB for the removal of CO<sub>2</sub> from the gas stream with higher flow rate owing to its high efficiency and its low cost.

### 1. Introduction

Ramshaw and Mallinson (1981) first presented that the concept of intensifying mass transfer was to establish a dramatically more rapid regeneration of the interface between gas and liquid phases. To attain this concept, they took advantage of centrifugal force to contact gas and liquid in a high centrifugal field by rotating doughnut-shaped packing element. Thus, a rotating packed bed (RPB) was developed for enhancing distillation and absorption efficiency. This novel technology was referred to as "Higee" (an acronym for high gravity). Under RPB operation, thin films and tiny droplets generated owing to a rigorous centrifugal acceleration (2000~10000 m/s<sup>2</sup>) could provide an enhancement in the gas-liquid mass transfer. Furthermore, the RPB could be operated higher gas and/or liquid flow rates owing to the low tendency of flooding relative to that in the conventional packed bed. Therefore, the gas-liquid mass transfer would frequently be enhanced by a factor of 10~100 and the dramatic reduction in the size of the equipment would be achieved, thereby reducing the capital and operating costs (Ramshaw, 1983). The RPB has been applied in a variety of applications

such as distillation (Lin et al., 2002), absorption (Lin et al., 2003), stripping (Lin and Liu, 2006), and ozone oxidation (Lin and Liu, 2003).

Although the gas absorption performance of a cross-flow RPB has been examined, the experimental results were isopropyl alcohol (IPA) absorption by water (Lin et al., 2006). The previous work (Lin and Chen, 2007) has applied a cross-flow rotating packed bed (RPB) to the removal of carbon dioxide ( $\text{CO}_2$ ) using absorption with NaOH solution. The experimental results indicated that MEA could provide the highest removal efficiency of  $\text{CO}_2$ . Based on these results, to increase the  $\text{CO}_2$  removal efficiency, the mixed amine solutions are considered to be the absorbent. Therefore, the objective of this work is to elucidate the removal of  $\text{CO}_2$  from gaseous streams by absorption with mixed amine solutions in a cross-flow RPB. PZ/MEA and PZ/AMP are adopted as the model mixed amine solutions in this work. The results in this work could provide further insight into the feasibility of applying a cross-flow RPB to the removal of  $\text{CO}_2$  from gaseous streams.

## 2. Experimental

Fig. 1 presents the experimental setup for absorbing  $\text{CO}_2$ . The  $\text{CO}_2$  concentration in the inlet  $\text{CO}_2$ - $\text{N}_2$  stream was set at 10 % (mole fraction). During normal operation, the  $\text{CO}_2$ - $\text{N}_2$  stream traveled axially from the bottom of the packing owing to the pressure drop. At the same time, the prepared mixed amine solution was introduced from the tank into the inner edge of the packing through a liquid distributor. mixed amine solution moved radially in the packing due to the centrifugal force and, then, exited the packing from the outer edge. Both  $\text{CO}_2$ - $\text{N}_2$  stream and mixed amine solution were in contact with the cross-flow mode within the RPB, in which  $\text{CO}_2$  in the  $\text{CO}_2$ - $\text{N}_2$  stream reacted with mixed amine in the liquid stream. The exiting  $\text{CO}_2$ - $\text{N}_2$  stream, containing low  $\text{CO}_2$  concentration, finally left the top of the packing, and, then, was discharged from the top of the RPB, while the  $\text{CO}_2$ -rich mixed amine solution was expelled from the bottom of the RPB.

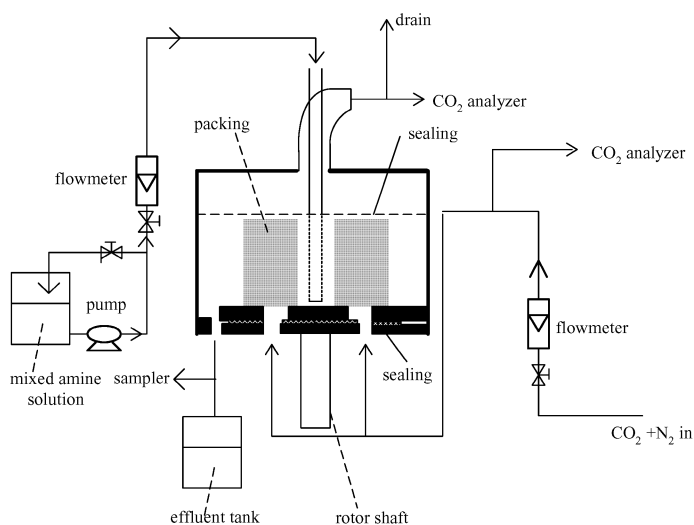


Fig. 1. Experimental setup of a cross-flow RPB for  $\text{CO}_2$  absorption process.

The cross-flow RPB had an inner radius of 2.4 cm, an outer radius of 4.4 cm, and an axial length of 12 cm. Stainless wire mesh was used as packings having a configuration of interconnected filaments with a mean diameter of 0.22 mm and an average mesh diameter of 3 mm and arranged within the cross-flow RPB where gas and liquid were contacted with the cross-flow mode. Packings had a specific surface area of  $677 \text{ m}^2/\text{m}^3$  and a voidage of 0.95. In general, the cross-flow RPB could be operated at the rotor speed of 600~1800 rpm, which provides 14~123 times gravitational force based on the arithmetic mean radius. During operation, the gas flow rate (axial direction) was varied at the range of 10~70 L/min and the liquid flow rate (radial direction) was varied at the range of 0.2~0.5 L/min. To prevent gas from bypassing the packing and keep the cross-flow operating mode, both sealings were adopted as shown in Fig. 1.

For most runs, a steady state was achieved within 10~15 min. The  $\text{CO}_2$  concentrations in the inlet and outlet  $\text{CO}_2\text{-N}_2$  streams were measured by an infrared (IR)  $\text{CO}_2$  analyzer (Ploytron, Draeger Ltd). The reproducibility tests under almost all of the operating conditions were carried out in this study. The  $\text{CO}_2$  concentration in outlet  $\text{CO}_2\text{-N}_2$  streams was observed to be reproduced with a deviation of less than 5%. Material balance on the inlet and outlet of both the gas and liquid streams presented that the errors were within 10%. All experiments were conducted at an average temperature of  $28^\circ\text{C}$  with atmospheric pressure.

### 3. Results and Discussion

The  $\text{CO}_2$  removal efficiency in a cross-flow RPB is defined as follows.

$$E = \frac{C_i - C_o}{C_i} \times 100 \quad (1)$$

where  $E$  is the  $\text{CO}_2$  removal efficiency, and  $C_i$  and  $C_o$  are the concentrations of  $\text{CO}_2$  in the inlet and outlet gas streams, respectively. The  $E$  values were measured at various values of the operation variables, including rotor speed ( $\omega$ ), gas flow rate ( $Q_G$ ), mixed amine flow rate ( $Q_L$ ), to estimate the  $\text{CO}_2$  absorption performance of a cross-flow RPB.

Fig. 2 summarizes the  $E$  values as functions of the rotor speed from 540 to 1600 rpm for three absorbents (0.2M PZ/0.8M MEA, 1.0M MEA, 0.2M AMP/0.8M MEA). These rotor speeds provided a centrifugal acceleration from 109 to  $955 \text{ m/s}^2$ . At a particular gas flow rate and liquid flow rate, increasing the rotor speed enhanced the  $E$  values, as expected, for three absorbents. This phenomenon revealed that the centrifugal force further increased the mass transfer rate of  $\text{CO}_2$  from the gas phase to the liquid phase during  $\text{CO}_2$  absorption. Similar to a countercurrent-flow RPB (Lin et al., 2003), a cross-flow RPB also could offer an enhancement in the gas-liquid interfacial area and a reduction in the resistance of  $\text{CO}_2$  mass transfer owing to that the thinner liquid films and/or the smaller droplets were induced by larger centrifugal force. Consequently, a cross-flow RPB should be considered to be an effective absorber for increasing  $\text{CO}_2$  absorption. Also, PZ/MEA provided the highest  $E$  values owing to that the reaction rate of  $\text{CO}_2$  with PZ/MEA was the highest. Moreover, the  $E$  values increased with mixed amine flow rate, however, decreased with the gas flow rate for three absorbents.

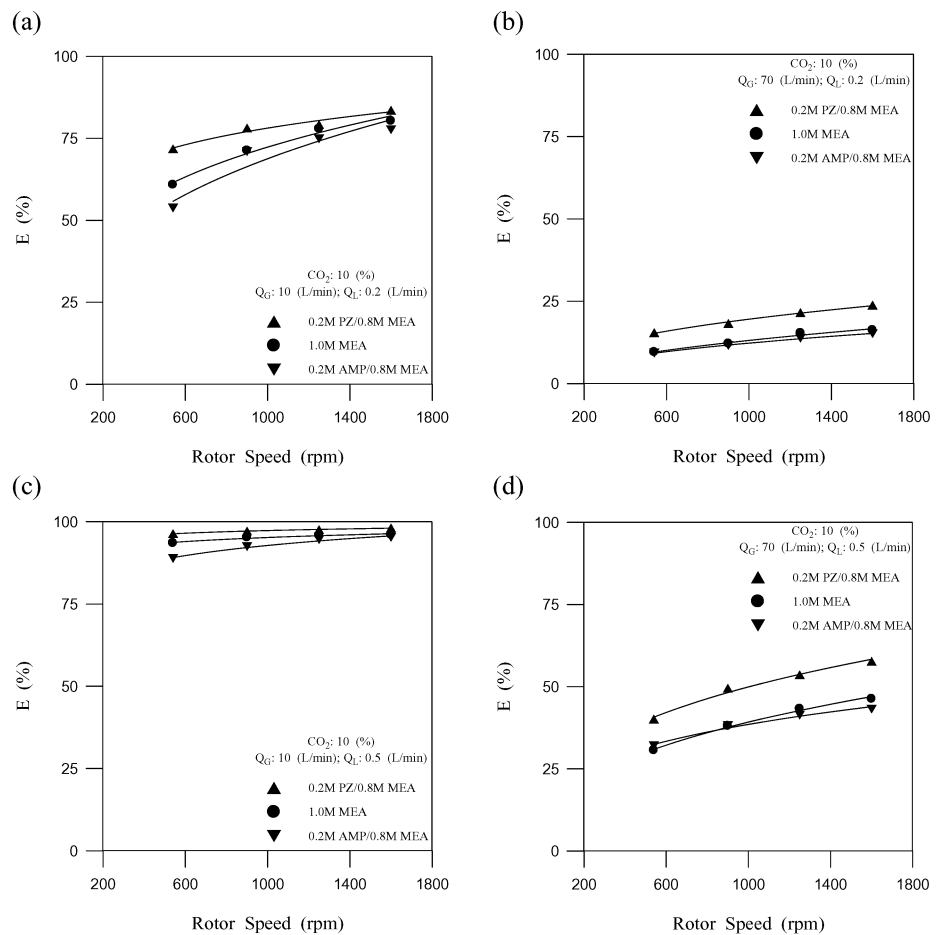


Fig. 2. Effect of rotor speed on  $E$  (a)  $Q_G = 10$  L/min and  $Q_L = 0.2$  L/min (b)  $Q_G = 70$  L/min and  $Q_L = 0.2$  L/min (c)  $Q_G = 10$  L/min and  $Q_L = 0.5$  L/min (d)  $Q_G = 70$  L/min and  $Q_L = 0.5$  L/min.

As shown in Fig. 2, it was noted that the  $E$  values was proportional to the rotor speed raised to the  $x$  power. The values of  $x$  depended on the gas flow rate, the mixed amine flow rate and the absorbent type as shown in Table 1. The  $x$  values at a low gas flow rate of 10 L/min Table 1 indicated that AMP/MEA offered the highest  $x$  values regardless of the liquid flow rate in the range of 0.2~0.5 L/min. This characteristic implied that for a low gas flow rate, the sensitivity of  $E$  to variations in the rotor speed for AMP/MEA was higher than those for other two absorbents. However, as the gas flow rate was increased to 70 L/min, this phenomenon was not observed, indicating that for a high gas flow rate, the sensitivity of  $E$  to variations in the rotor speed for MEA was higher than those for other two absorbents. For a given absorbent, the highest  $E$  value was found at a low mixed amine flow rate of 0.2 L/min and a high gas flow rate of 70 L/min, implying that the rotor speed could compensate the loss of removal efficiency induced by low mixed amine flow rate and high gas flow rate.

*Table 1 Variation of exponent x with various operating conditions*

| Q <sub>G</sub><br>(L/min) | Q <sub>L</sub><br>(L/min) | x                |          |                   |
|---------------------------|---------------------------|------------------|----------|-------------------|
|                           |                           | 0.2M PZ/0.8M MEA | 1.0M MEA | 0.2M AMP/0.8M MEA |
| 10                        | 0.2                       | 0.131            | 0.263    | 0.339             |
| 10                        | 0.5                       | 0.016            | 0.026    | 0.066             |
| 70                        | 0.2                       | 0.403            | 0.509    | 0.461             |
| 70                        | 0.2                       | 0.331            | 0.386    | 0.280             |

#### 4. Conclusion

This work has examined the absorption performance of a cross-flow RPB with the removal of CO<sub>2</sub> by mixed amine solutions from gaseous streams. The results were considered in relation with the removal efficiency, E values. As expected, increasing the rotor speed increased the E values; however, an optimum compromise between the consumption of energy (rotor speed) and the removal efficiency must be evaluated for industrial-scale applications.

According to the experimental results, CO<sub>2</sub> removal efficiency of increased with rotor speed and mixed amine flow rate, but decreased with an increase of gas flow rate. Moreover, CO<sub>2</sub> removal efficiency using PZ/MEA was superior to those using MEA and AMP/MEA. Consequently, PZ/MEA could be used in a cross-flow RPB for the removal of CO<sub>2</sub> from the gas stream with higher flow rate owing to its high efficiency and its low cost.

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