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Abstract—This paper deals with the modeling and control of the air temperature and humidity in greenhouses. A physical model of the greenhouse used in the Simulink/Matlab environment is elaborated to simulate both temperature and indoor humidity. As a solution to the non-linearity and complexity of the greenhouse system, a fuzzy logic method is developed to control the actuators that are installed inside the greenhouse for heating, ventilation, humidification and cooling to obtain a suitable microclimate.

Keywords-greenhouse; fuzzy logic controller; air temperature; humidity; Simulink; Matlab

I. INTRODUCTION

Agricultural production is a central economy field in many countries. Tunisia is considered one of the best worldwide agricultural product exporters. Nowadays, greenhouse is the main solution to climate change effects. Its main purpose is to effectively control the environment and protect the plants by creating a favorable climate. Among the conditions in a greenhouse, this paper focuses on indoor temperature and humidity. An optimal vegetation yield can be produced from the precise configuration of these conditions [1]. Numerous methods of greenhouse control have been studied and developed. The regulations inside the greenhouse consist of evaporation, fogging and ventilation systems. This paper presents a control system useful for adaptation despite the nonlinearity and complexity of greenhouse dynamics [2, 3]. Various types of climate control greenhouse systems have been previously mentioned. In [4, 5], a feedback controller approach has been discussed. The type of climate control mentioned in [6] has been developed to the optimal control method. Neural networks were studied in [7-9]. Authors in [10, 11] offer a regulation of temperature and humidity inside the greenhouse with a fuzzy logic regulator. In [12], the Takagi-Sugeno method of the air temperature control is described. In [13-15],

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model predictive control (MPC) was used. The proposed work starts with the simulation of the dynamic greenhouse model followed by its validation and its control via Fuzzy Logic.

II. GREENHOUSE MODEL

The model of the proposed input-output system can be seen in [16]. The considered variables are: T_{int} is the interior temperature and H_{int} is the humidity variable. The adjustment of these variables will be obtained by MV_{α} which is the ventilation system, MV_w which is the heating system, and MV_{fog} which is the fogging system. The measurable disturbances consist of wind speed, solar radiation, and outside humidity and temperature [16].

A. Proposed Model

The first step of the proposed study is the development of the dynamic model of the greenhouse using the Simulink/Matlab. Many physical models like the energy balance and mass balance have been suggested to describe the dynamics of the greenhouse climate [17, 18].

B. Greenhouse Model with Simulink

A derived simple model is required to design a control system that analyzes and guesses the correct variables of cooling, heating and ventilation systems. The model consists of conventional dynamic equations that correspond to the indoor air temperature T_i , soil temperature T_m , and indoor humidity X_i [17]. The differential equations are given by the heat and humidity balance.

1) Heat Balance

The dynamic model of the air temperature and the thermal mass temperature inside the greenhouse are described by (1)

Corresponding author: Manel Jomaa

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Vol. 9, No. 4, 2019, 4405-4410

and (9) [17]:

$$v_i \rho c_p \frac{dT_i}{dt} = Q_s - Q_{cc} + Q_m - C_{sat}(Q_e + Q_n) - Q_v + W$$
(1)

where:

 Q_s is the solar energy supplied to the air volume determined by (2):

$$Q_s = A_i \pi S_0 \tag{2}$$

 Q_{cc} is the energy exchange by the conduction and the convection phenomena that are explained using (3):

$$Q_{cc} = A_i A_c (T_i - T_o) \tag{3}$$

 Q_m is the energy exchange between the thermal mass and the inside air determined by (4):

$$Q_m = A_i h_m (T_m - T_i) \tag{4}$$

 Q_e is the energy loss due to the crop evapotranspiration:

$$Q_e = \lambda E \tag{5}$$

 Q_n is the energy loss by the nebulization:

$$Q_n = \lambda fog \tag{6}$$

 Q_{v} is the energy exchange due to the window ventilation:

$$Q_v = \rho c_p G(T_i - T_o) \tag{7}$$

W is the energy provided from the heating system:

$$W = \frac{MV_w}{100} W_{\text{max}} \tag{8}$$

The thermal mass temperature inside the greenhouse is described by (9):

$$A_i C_m \frac{dT_m}{dt} = Q_{sm} - Q_m - Q_f \tag{9}$$

Knowing that:

$$Q_{sm} = \alpha_m Q_s \tag{10}$$

Equation (10) is the energy stored by the thermal mass during the day and (11) is the energy loss through the ground:

$$Q_f = A_i k_a \left(\frac{T_m - T_{ref}}{Z_{ref}} \right) \tag{11}$$

2) Humidity Balance

The model of the relative humidity inside the greenhouse is determined by (12) [17]:

$$\sigma V_i \frac{dX_i}{dt} = F_v + C_{sat} \left(E + fog \right)$$
(12)

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where:

 F_{v} is the water rate in the air renewal flow:

$$F_{v} = \rho G \left(X_{o} - X_{i} \right) \tag{13}$$

E is the crop evapotranspiration identified by (14):

$$E = \frac{A_i \left(\Delta R_n + 2L\rho c_p D_i gwb \right)}{\left(\Delta + \gamma \left(1 + \left(\frac{gwb}{gws} \right) \right) \right) \lambda}$$
(14)

fog is the water rate of the fogging system:

$$fog = \left(\frac{MV_{fog}}{100}\right) fog_{\max}$$
(15)

The greenhouse that is used for the validation is situated at the C.R.T.EN Borj Cedria Park of science and technology in Tunisia, in a semi-urban environment. The greenhouse axes are in the East-West direction. The dimensions are 12.5m length, 8m width and 3m height. The acquisition of both external weather conditions (wind speed, temperature, radiation, and humidity) and internal climate greenhouse data are connected to a Campbell 21X data logger. The measurements of external and internal relative humidity are performed via HMP35C sensors with 3% precision and a range between 0% and 100%. The external and internal temperatures are measured in a range from -35°C to +50°C. The solar radiation is measured by a pyranometer with 5% precision [3]. Figure 1 shows the solar radiation measured in the 29th, 30th and 31st of March, 2001 whereas Figure 2 presents the wind speed, measured at the same dates.





Figures 3-5 present the simulation results, for the same time period, of internal air temperature (K), internal soil temperature (K) and relative humidity (%).

Jomaa et al.: Greenhouse Modeling, Validation and Climate Control based on Fuzzy Logic



Fig. 3. Simulation results of the air temperature inside the greenhouse



Fig. 4. Simulation results of the soil temperature inside the greenhouse



Fig. 5. Simulation results of the relative humidity inside the greenhouse

The simulated results obtained via Simulink are compared with the detailed model discussed and described in [3]. The same parameters of the greenhouse are used in both cases.



Figure 6 presents the simulated and measured indoor air temperature. Figure 7 shows the simulated and measured results of the indoor relative humidity. It can be seen that a

good agreement is obtained between the simulated and the measured results of both temperature and relative humidity. In order to activate the actuators, power should be supplied. In this case, a logic control is selected and its pseudo-code is briefly described in Figure 8. Figures 9-11 present the heating, ventilation and humidifying rates that are delivered by the control algorithm in Figure 8.



Fig. 8. Algorithm block diagram



III. FUZZY LOGIC CONTROLLER

Fuzzy logic has been considered an attractive solution for various engineering problems due to features such as its robustness, simplicity and flexibility. Three stages must be satisfied to design this type of control system: Fuzzification, inference rules and defuzzification [20]. The main aim of this system is to control the climate inside the greenhouse and boost its effectiveness.

A. The Structure of The Control System

The input variables of temperature and humidity in the fuzzy logic controller are represented by ΔT with outside temperature and ΔH with outside humidity knowing that:

$$\Delta T = T_{desired} - T_{indoor} \in (NB, NM, Z, PM, PB)$$
(16)

where outside temperature \in (PM, Z, PG).

$$\Delta H = H_{desired} - H_{indoor} \in (NB, NM, Z, PM, PB)$$
(17)

and outside humidity \in (PM, Z, GP)

	NB : Negative _ Big	
where	NM : Negative _ Medium	[PM : Positive_Medium]
	Z : Zero	{Z : Zero
	PM : Positive _ Medium	PB: Positive_Big
	PB : Positive _ Big	

The methodology described in Figure 8 was used to develop this command. During the control we took into account the external environmental conditions (outside temperature and outside humidity). The output variables are the heating rate (Heating), the ventilation rate (Ventilation) and the humidifying rate (Humidifying).

(Heating, Ventilation) \in (Zero, Medium, High)

(Humidifying) \in (Zero, Medium, High)

The fuzzy inference method that is used in this work is the Mamdani method and the defuzzification technique is based on the center of gravity method.

B. Decoupling Fuzzy Logic Controller

Figure 12 presents the input variables of the temperature and outside temperature and Figure 13 presents the input variables of the humidity and outside humidity. Figure 15 presents the output variables of heating, ventilation and humidifying rates.

IV. SIMULATION RESULTS

The main objective of control is to smoothly regulate air temperature and humidity inside the greenhouse to their desired values ($T_{desired}$, $H_{desired}$). We controlled the actuators by lowering their rates in order to reduce energy. The value of the desired temperature is 15°C at night and 28°C at day. The desired relative humidity inside the greenhouse are illustrated in Figures 15 and 16 during simulation time of one day.



Vol. 9, No. 4, 2019, 4405-4410

Fig. 12. Membership functions of temperature error (ΔT) and outside temperature



Fig. 13. Membership functions of humidity error (ΔH) and outside humidity



Fig. 14. Membership functions of heating, ventilation and humidifying rates



Fig. 15. Simulation results of the greenhouse temperature with fuzzy logic controller



Fig. 16. Simulation results of the greenhouse humidity with fuzzy logic controller

The provided heating and ventilation rates are displayed in Figures 17 and Figure 18. A regulator fuzzy logic controller is applied to control the humidifying system in order to regulate the relative humidity at its set point value, as presented in Figure 19.



V. CONCLUSION

In this article, a greenhouse model has been proposed and validated. A comparison between the simulated and measured results of the internal air temperature and the relative humidity has been made using the parameters proposed in [3]. A good agreement has been obtained between the calculated and measured data, which indicates the efficiency of the proposed model. Based on this model, a fuzzy logic controller has been developed to satisfy the demands in terms of temperature and humidity, using the measured data. The results showed a stable behavior of both temperature and humidity with a low rate of heating, ventilation and humidification. This behavior has been achieved without using the dehumidifier system in order to reduce energy consumption. In the future, we will focus on developing an improved control model for the greenhouse climate and testing the stability and robustness of the fuzzy logic controller with more variables representing the complete state of the greenhouse. In addition, we will design a power system based on renewable energy sources in order to reduce the use of grid utilities.

NOMENCLATURE

4 [m ²]	Windows area [50m ²]	
7	Constant for renewal volumetric flow	
4_c	Loss coefficient of conduction and convection	
$4_i [m^2]$	Greenhouse surface area [100m ²]	
C_m	Thermal mass heat capacity	
$Cp [J Kg^{-1} \circ C^{-1}]$	Air heat capacity [1003J·Kg ⁻¹ °C ⁻¹]	
Cs _{at}	Air saturation coefficient	
D_i [kpa]	Air water vapor deficit	
$E \left[kg_{H20} S^{-1} \right]$	Crop evapotranspiration	
$\log[kg_{H20}S^{-1}]$	Water rate of fogging system	
$Fv [kg_{H20}S^{-1}]$	Water rate in the air renewal flow	
$G[m^{3}S^{-1}]$	Renewal air flow	
$zwb [mS^{-1}]$	Boundary-layer conductance	
$zws [m S^{-1}]$	Stomatal conductance	
hm [W m ⁻¹ K ⁻¹]	Conductivity coefficient between air and thermal mass	
H_i [%]	Inside relative humidity	
H_{o} [%]	Outside relative humidity	
L	Leaves area index	
MV_{fog} [%]	Fogging system manipulated variable	
$MV_w[\%]$	Heating system manipulated variable	
$MV_{\alpha}[\%]$	Windows opening manipulated variable	
o _{sat} [kPa]	Saturation pressure	
p [kPa]	Atmospheric pressure [98.1kPa]	
	Energy exchange by conduction and convection	
200 [W]	phenomena	
Qe [W]	Energy loss due to crop evapotranspiration	
Qf[W]	Energy loss through ground	
Qm [W]	Energy exchange with thermal mass	
Qn [W]	Energy loss by nebulization	
Qs [W]	Solar energy supplied to air volume	
Qsm [W]	Energy stored by thermal mass during the day	
Qv [W]	Energy exchange due to window ventilation	
$Rn [W m^{-2}]$	Solar radiation absorbed by the crop	
So [W m ⁻²]	Solar radiation	
Ti [°C]	Inside temperature	
Tm [°C]	Thermal mass temperature	
To [°C]	Outside temperature	
Tref [°C]	Ground temperature at reference depth	
Vi [m²]	Greenhouse volume [300m ³]	
$V[ms^{-1}]$	Wind speed	
W[W]	Energy from the heating system	
Wmax [W]	Maximum power of the heating system	
<i>Xi</i> [kg _{H20} kg _{air} ⁻¹]	Inside absolute humidity	

Jomaa et al.: Greenhouse Modeling, Validation and Climate Control based on Fuzzy Logic

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Xo [kg _{H2O} kg _{air} ⁻¹]	Outside absolute humidity
Xsat [kg _{H2O} kg _{air} ⁻¹]	Absolute saturation humidity
Zref [m]	Reference depth
α[°]	Opening window angle
⊿ [kPa °C ⁻¹]	Slope of water vapor saturation
γ [kPa °C ⁻¹]	Psychometric constant
λ [J Kg ⁻¹]	Latent heat of vaporization
$\rho [Kg_{air} m^{-3}]$	Air density [1.25 Kg _{air} m ⁻³]
τ	Transmission coefficient of the greenhouse

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