Modeling of Antenna for Deep Target Hydrocarbon Exploration

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ABSTRACT

Nowadays control source electromagnetic method is used for offshore hydrocarbon exploration. Hydrocarbon detection in sea bed logging (SBL) is a very challenging task for deep target hydrocarbon reservoir. Response of electromagnetic (EM) field from marine environment is very low and it is very difficult to predict deep target reservoir below 2km from the sea floor. This work premise deals with modeling of new antenna for deep water deep target hydrocarbon exploration. Conventional and new EM antennas at 0.125Hz frequency are used in modeling for the detection of deep target hydrocarbon reservoir. The proposed area of the seabed model (40km 40km) was simulated by using CST (computer simulation technology) EM studio based on Finite Integration Method (FIM). Electromagnetic field components were compared at 500m target depth and it was concluded that Ex and Hz components shows better resistivity contrast. Comparison of conventional and new antenna for different target depths was done in our proposed model. From the results, it was observed that conventional antenna at 0.125Hz shows 70%, 86% resistivity contrast at target depth of 1000m where as new antenna showed 329%, resistivity contrast at the same target depth for Ex and Hz field respectively. It was also 355% investigated that at frequency of 0.125Hz, new antenna gave 46% better delineation of hydrocarbon at 4000m target depth. This is due to focusing of electromagnetic waves by using new antenna. New antenna design gave 125% more extra depth than straight antenna for deep target hydrocarbon detection. Numerical modeling for straight and new antenna was also done to know general equation for electromagnetic field behavior with target depth. From this numerical model it was speculated that this new antenna can detect up to 4.5 km target depth. This new EM antenna may open new frontiers for oil and gas industry for the detection of deep target hydrocarbon reservoir (HC).

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Keywords: Bentonite, Portland cement, Strength of moulding sand

I. Introduction

Sea bed logging is an application of control source electromagnetic method which is used to locate an oil reservoir beneath the sea floor by measuring electromagnetic fields [1-4]. In typical control source method a horizontal electric dipole antenna is towed by a surface vessel at a short distance 30m above from the sea floor [5-7]. Dipole antenna transmits very low frequency electromagnetic waves with frequency ranges from 0.25Hz-10Hz due to low frequency transmitted energy propagates down through the subsurface [8-10]. Low frequency electromagnetic waves attenuate more in the conductive layer and less in the resistance layer due to the skin depth. In a large resistive layer such as hydrocarbon electromagnetic energy flows along the reservoir (described as guided wave) is detected by the stationary sea floor electric or magnetic field detectors which are deployed on the sea floor. Control source electromagnetic method depends on the resistivity of the hydrocarbon and surrounding sediments. Hydrocarbon in the sea bed has resistivity of few tens to hundred ohm meter (30Ω m- 500Ω m), sea water (0.5Ω m- 2Ω m) while all other layers including sediments in the sea have resistivity $(1 \ \Omega m - 2 \ \Omega m)$ [11-17]. In deep water the air wave effect is negligible so the wave guided back from the hydrocarbon can predict the presence of hydrocarbon [18]. Target depth is also very important in sea bed logging. Frequency and offset plays an important role to determine target depth. Shallow targets shows measurable response at near offset with high frequency where as deep targets at large offset with low frequency. G. Michael Hoversten reports that simulated oil-water contact at 2 km depth below the sea floor shows a response below the expected noise levels. The resistivity model in which maximum target depth response measured was 3km for 8km offset [19]. Multiple frequency range of electromagnetic waves is used to improve control source electromagnetic data for deep target hydrocarbon reservoir.



Deep target having variable size and depth can cause the risk factor so high and low frequency reduces this risk factor. Deep water field survey in Nigeria two fundamental frequencies (0.05Hz and 0.25Hz) with higher frequency are used which shows very promising survey results. For shallow target depth 0.25Hz frequency and the first two harmonics is useful to detect the thin resistive hydrocarbon reservoir. Low frequency (0.05Hz) data provide useful information about 2km resistivity background model. This wide range of multiple frequencies is used to reduce the drilling risk factor [20]. Direct detection of hydrocarbon which is deeply buried can be done by subsea EM sounding technique. Survey was done across TWGP, Norway offshore and they found the target at the depth of 1100m below the sea floor was reported [21]. Transmitter height changing above the sea floor was investigated in a noise model and also included the data which create uncertainty by changing the transmitter height. Inversion of the data with multilayers and four layers models was done. It was observed that this model can detect the resistive layer at a depth of 1500-1600m below the sea floor for control source CSEM electromagnetic method where as 2km depth for seismic method [22]. Propagation of electromagnetic (EM) waves travelling in seawater can be predicted by using Maxwell's equations. If the propagating of electromagnetic wave in the y direction then it can be described in terms of the electric field strength Ex and the magnetic field strength Hz [23].

$$E_X = E_0 \exp(j\omega t - \gamma y) \tag{1}$$

$$H_s = H_0 \exp(j\omega t - \gamma y) \tag{2}$$

$$\gamma = j\omega \sqrt{\varepsilon\mu - j\frac{\omega\mu}{\omega}} = \alpha + j\beta$$
⁽³⁾

Where (γ) is the propagation constant, (ε) permittivity, (μ) permeability, (σ) conductivity, α attenuation factor, β phase factor and $\omega = 2\pi f$ the angular frequency as given in equation (3). Electromagnetic wave propagation can be described by a wave number K as given in equation 4.

$$K = \omega \sqrt{\mu \omega + \frac{i\mu \omega}{\omega}} = \frac{\omega}{c_p} + \frac{i}{\delta}$$
⁽⁴⁾

Where k is the wave number and $i=\ddot{O}-1$ is the complex number, Cp phase velocity and \Box is the skin depth. First term in equation (4) inside the square root represent the displacement current and second term represent conduction current in Maxwell's equation.

Numerical model is a very important to know the location hydrocarbon in sea bed logging. It can provide the information about the target depth at which target depth the electromagnetic wave signal provide information about hydrocarbon reservoir [24].

 Table 1.
 Simulated model parameters with different resistive layers (air, sea water, overburden and under burden)

Target depth	Air thickness	Under burden	Hydro- carbon	Sea Water depth	Frequency
(m)	(m)	(m)			(Hz)
	500	4500	100	2000	0.125
	500	4250	100	2000	0.125
_	500	4000	100	2000	0.125
	500	3750	100	2000	0.125
	500	3500	100	2000	0.125
	500	3250	100	2000	0.125
Up to 4500	500	500	100	2000	0.125

Material parameters	Air	Sea water	Under Burden/ Over Burden	Hydrocarbon
Conductivity	1.006	80	30	4
Relative Pemittivity	1.0e-11	4	1.5	0.001
Thermal conductivity	0.024	0.593	2	0.492
Density	1.293	1025	2600	900

 Table 2.
 Relative permittivity, conductivity values of air, sea water Overburden/under burden and hydrocarbon

This work premise deals with the study of electromagnetic field components, conventional and new antenna electromagnetic field comparison for deep target hydrocarbon reservoir detection. New antenna electric field data of different curvatures is used for numerical model to know the exact target depth with this new antenna design.

II. Methods.

We use CST (Computer simulation technology) software for finite integration method (FIM). Computer simulation technology (CST) is used to discritize each Maxwell's equations at low to investigate the resistivity contrast. Forfinite integration technique, Computer frequency simulation technology software is used as a tool for low frequency to solve any problem. FIM was used to detect deep target hydrocarbon below 3000m from seafloor by using CST software. CST software was used to detect deep target hydrocarbon between 1000m to 400m underneath seabed. Model area was assigned as 40'40 km to replicate the real seabed environment with various target positions. Environment with and without hydrocarbon were also prepared for comparison purpose later. There were few steps involved in generating the CST simulated model. First step was to set parameters for aluminium antenna. In this case we used length of 270m, frequency of 0.125Hz and current of 1250A. Second step was to set parameters for the model. Airthickness was set as 500m, sea water depth of 2000m, overburden thickness of 1000m, hydrocarbon thickness of 100m and under burden with their different conductivities and permeability values (Table 2). Thickness of the overburden was increased as the target depth varied gradually (every 250m) from 500m to 5000m. Third step was to apply electric boundary conditions (Table 1). Fourth step was to run low frequency full wave solver to simulate sea bed model. The final step was post processing to generate the simulated data for results analysis at different target depths. Maxwell's equations for magnetic and electric fields are used as a code in the software to get electric and magnetic field response with and without HC. Schematic diagram of proposed seabed model with CST simulated model is shown in Figure 1.

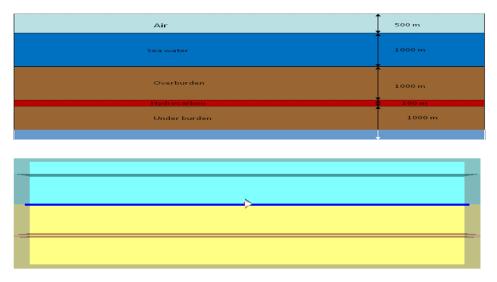
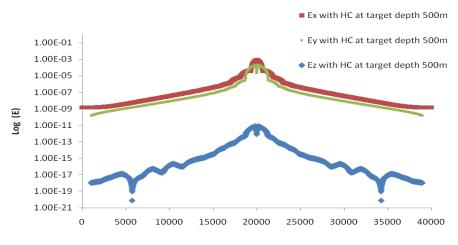


Fig. 1. (a) Schematic diagram of proposed model and (b) CST simulated model

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Source receiver offset (m)

Fig. 2. Comparison of E-filed components (Ex, Ey, Ez) response at 500m target depth

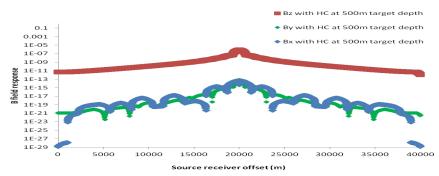


Fig. 3. Comparison of B-filed components (Bx, By, Bz) response at 500m target depth

III. Results and discussion.

Electromagnetic field components response from hydrocarbon reservoir in sea bed logging is very important to show better resistivity contrast. In sea bed logging both electric and magnetic field sensors are placed on the sea floor to record the electromagnetic field data. Electromagnetic field data consists of three components i.e. (x, y, and z). Choice of the electromagnetic field components depends on the electromagnetic waves propagation. All three components of electric field response were measured with conventional HED antenna within the proposed area (40 km x 40km). Components study was done in deep water (2000m) where no air waves effect take place. Comparison of E-field components is given in Figure 2. Ex component shows better E field response at 500m target depth as compared to Ey and Ez.

Magnetic field components comparison was also done to know which component gave high magnetic field response with the presence of hydrocarbon reservoir. Magnetic field strength is although lower than the electric field strength but it is also very important for hydrocarbon prediction but only for shallow target where as for deep target the signal strength is very low which cannot be able to predict the presence of hydrocarbon reservoir. Magnetic field comparison is given in Figure 3. Bz component gave higher magnetic field response with the presence of hydrocarbon reservoir at 500m depth. H- field response was also analyzed at 500m target depth is given in Figure 4. H-field response of all three components was recorded and plotted to know which component gave higher response. Hz component shows better response with the presence of hydrocarbon reservoir than Hx and Hy. Selection of E, B and H field components was done and it was conclude that Ex, Bz and Hz gave better delineation of hydrocarbon reservoir at 500m target depth.

Finally Ex, Bz and Hz electromagnetic field components were plotted as given Figure 5. From these results, it was observed that the Ex and Hz components gave better delineation of hydrocarbon reservoirs according to Maxwell's equations; if the electromagnetic wave is propagating in y direction then Ex and Hz components gave better delineation of hydrocarbon reservoirs [25]. These two components were chosen for deep target hydrocarbon detection with straight and new antenna.

A. Straight antenna MVO Results

Straight antenna magnitude verses offset data was plotted to compare with new antenna in full scale sea bed logging environment. Conventional antenna and new antenna length, frequency and model were kept same to check the performance of new antenna for deep water-deep target.

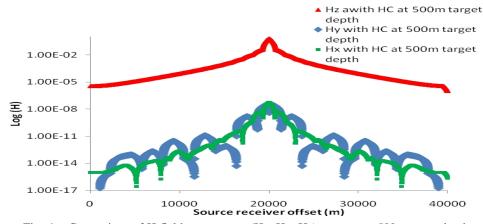


Fig. 4. Comparison of H-field components (Hx, Hy, Hz) response at500m target depth

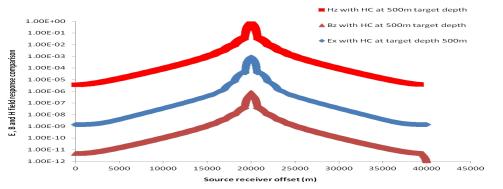
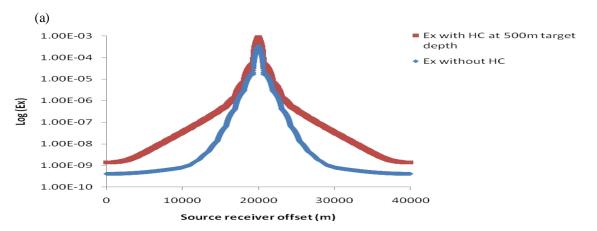
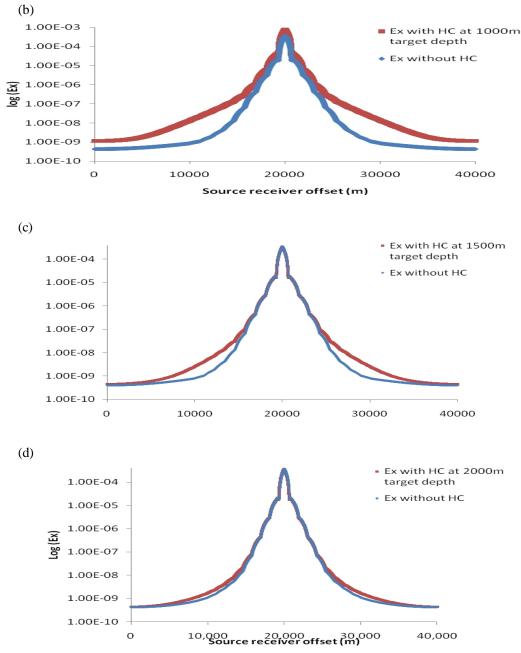
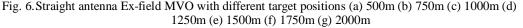


Fig. 5. Comparison of Hz, Ex and Bz field response at 500m target depth

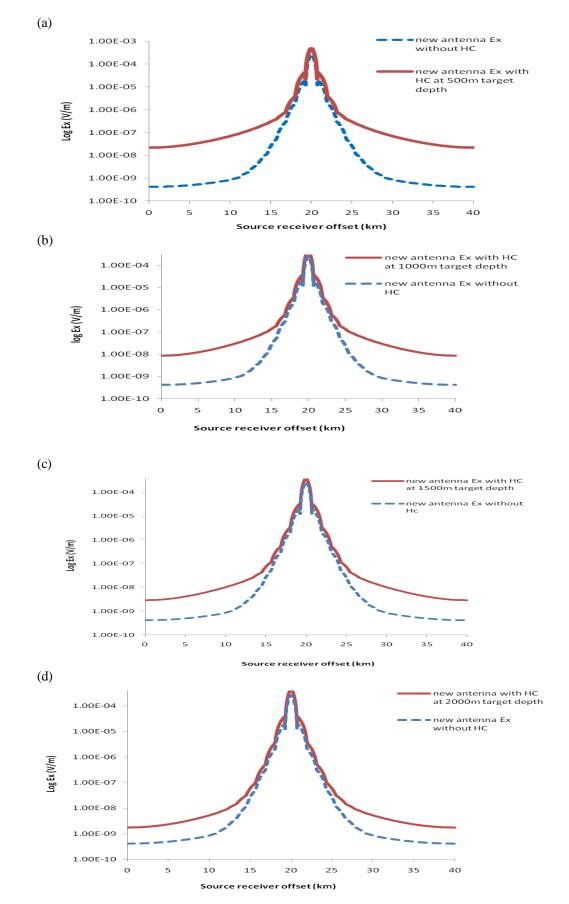


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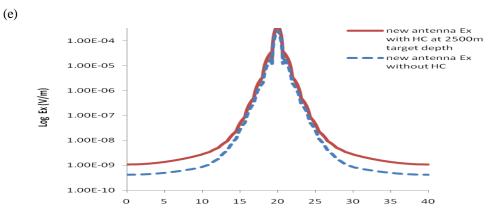




Straight antenna magnitude verses offset data was plotted by changing the target depth from 500m until 2000m. Ex field response with and without hydrocarbon was measured to know the exact target depth which can be detected by the straight HED antenna in deep water. At 500m target depth straight antenna shows 70% resistivity contrast is given Figure 6 (a). Target depth was varied from 500m to 750m but the simulated model total layers depth keep constant by reducing the under burden depth. Ex field response decreases by increasing the target depth due to the skin depth. At 750m target depth resistivity contrast drops to 57% is shown Figure 6b). Ex field response was measured until no hydrocarbon detected. It was analyzed that 42%, 26% and12% difference with and without hydrocarbon at 1000m, 1250m and 1500m respectively. Further target depth was decreased from 1500m to 2000m the difference between with and without hydrocarbon reservoir is 5% and 2% which is less than 10%. Straight antenna can detect up to 1500m target depth below the sea floor because drilling risk factor is involved below 10%.

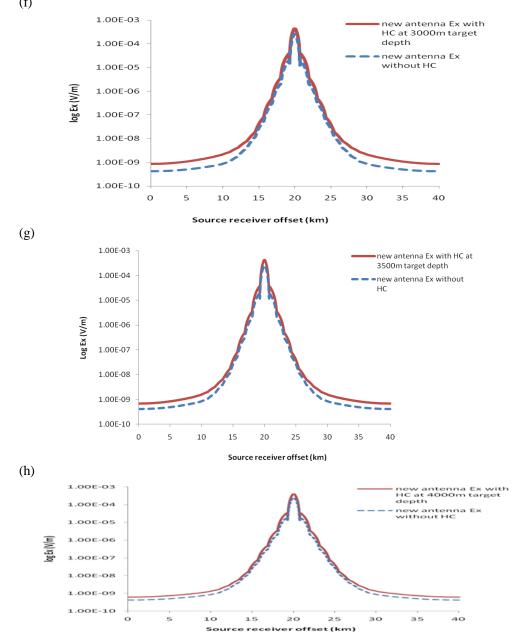


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(f)

Source receiver offset (km)



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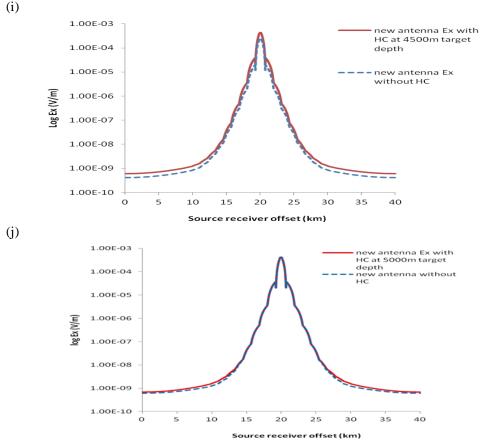


Fig. 7.New antenna Ex-field MVO with different target positions (a) 500 m (b) 1000 m (c) 1500 m (d) 2000 m (e) 2500 m (f) 3000 m (g) 3500 m (h) 4000 m (i) 4500 m (j) 5000 m

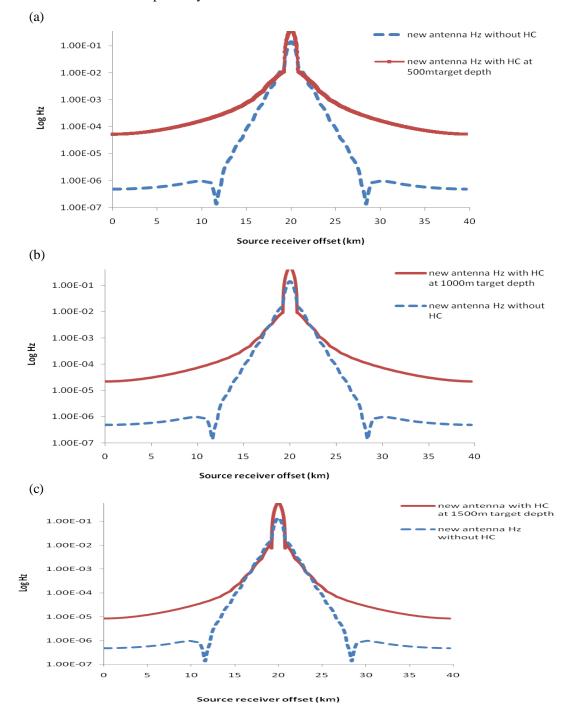
Hz field response was also measured with straight antenna to get better delineation of hydrocarbon reservoir. Analysis between Ex and Hz at 500m target depth shows 16% better delineation of hydrocarbon reservoir than Ex field response. At 1500m target depth Hz field response was 12% higher than Ex field response. It was also conclude that Hz field shows 10% difference at 1750m target depth. Magnetic field Hz component able to detect the hydrocarbon reservoir at 1750m target depth where as Ex field response for 1500m target depth respectively. Due to high H-field strength it can detect 250m extra depth than Ex field response is given Figure 7. Below 2000m strong electromagnetic signal strength is required for deep target hydrocarbon detection.

B. New antenna MVO results

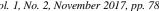
Deep target detection is a challenging task in sea bed logging. Response from deep target hydrocarbon reservoir is very weak from straight antenna. The guided wave from the high resistive deep target has very low signal strength which is very difficult to predict the presence of hydrocarbon reservoir. A strong EM field is required and some modification of the HED antenna is highly needed by the oil and gas industry to ensure deep target. To enhance the signal strength and focus more electromagnetic (EM) waves for deep target new antenna was simulated with and without the presence of hydrocarbon reservoir to check the performance of new antenna. The proposed area of the seabed model which was simulated by using CST (computer simulation technology) EM studio based on Finite Integration Method (FIM). New antenna has the ability to focus electromagnetic waves.

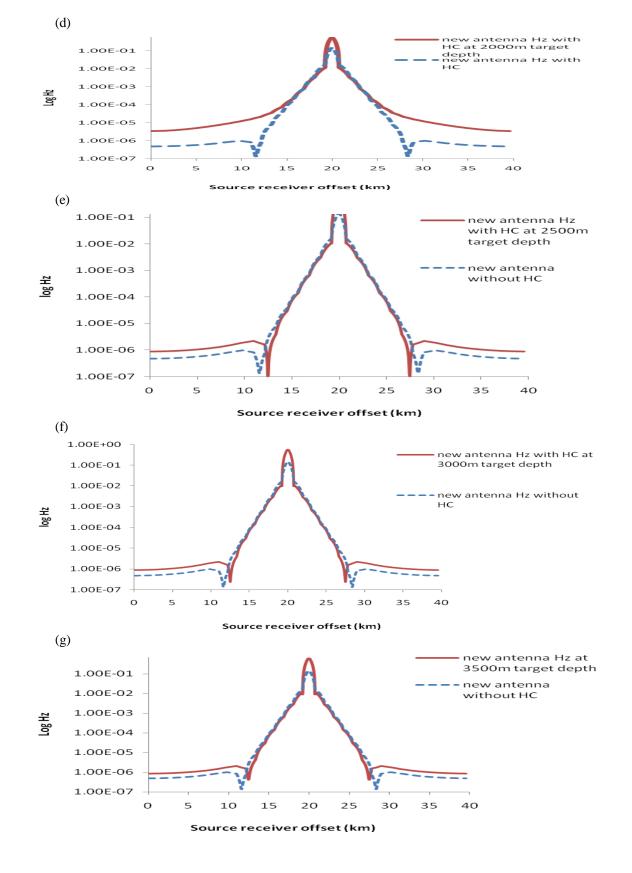
New antenna was used to get the magnitude verses offset (MVO) response for 4000m target depth as given Figure 7. Solid lines indicate the response with presence of hydrocarbon where as dotted line represents without hydrocarbon response. It was analyzed that this new antenna shows 510% difference between the hydrocarbon or without hydrocarbon at 500m target depth than

straight antenna. This difference motivates to go for further target depth to predict the presence of high resistive layers hydrocarbon (HC). New antenna Ex field response shows 46% difference between with and without hydrocarbon resrvior at 4000m target depth is given Figure 8. This new antenna shows 12% difference at 4250m target depth in deep water and can be used to reduce the drilling risk factor for oil and gas industry until 4250m target depth. Comparison of straight and new antenna is shown in Table 3 and Table 4 respectively. the presence of high resistive layers hydrocarbon (HC). New antenna Ex field response shows 46% difference between with and without hydrocarbon resrvior at 4000m target depth is given Figure 8. This new antenna shows 12% difference at 4250m target depth is given Figure 8. This new antenna shows 12% difference at 4250m target depth is given Figure 8. This new antenna shows 12% difference at 4250m target depth is given Figure 8. This new antenna shows 12% difference at 4250m target depth. Comparison of straight and mithout hydrocarbon resrvior at 4000m target depth is given Figure 8. This new antenna shows 12% difference at 4250m target depth in deep water and can be used to reduce the drilling risk factor for oil and gas industry until 4250m target depth. Comparison of straight and new antenna is shown in Table 3 and Table 4 respectively.



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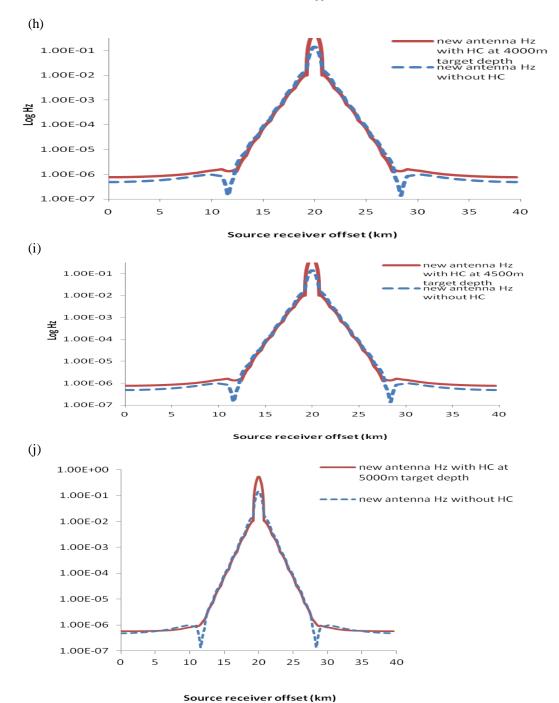


Fig. 8. New antenna Hz-field MVO with different target positions (a) 500m (b) 1000m (c) 1500m (d) 2000m (e) 2500m (f) 3000m (g) 3500m (h) 4000m (i) 4500m (j) 5000m.

New antenna Hz magnitude verses offset comparison with different target depth is given Figure 8. Solid lines in MVO plot represent hydrocarbon response where as dotted lines without hydrocarbon reservoir. For near offset less than 3km direct wave dominate and hydrocarbon reservoir presence cannot be predicted. Greater than 3km offset in deepwater guided response dominate the direct wave's response. Due to this reason greater than 3km offset can predict about the presence of hydrocarbon reservoir. Magnetic field response curve width is more as compared to electric field because magnetic field decreases 1/R2 where as electric field 1/R3 (R is the radial distance from the center of dipole to the measurement point) [26]. At 500m target depth new antenna shows 540% Hz field strength than without hydrocarbon reservoir. As the target depth

increases the Hz field strength decreases due to the skin depth effect. At 4250m target depth Ex response was 12% where as Hz 16% with new antenna design and Hz component able to delineate deep target better than Ex component. Analysis of new antenna results reveals that it can be used to detect deep target up to 4500m target depth below the sea floor in deep water.

Table 3. Straight antenna Exand Hz field response % difference comparison at different target depth with and without HC

Target Depth (m)	Straight antenna % difference in Ex field with and without HC at different target depth	Straight antenna % difference in Hz field with and without HC at different target depth
500	70	84
750	57	76
1000	42	58
1250	26	40
1500	12	22
1750	5	10
2000	2	5

Table 4.	At different ta	arget depth	with and	without HC

Target Depth (m)	New antenna % difference in Ex field with and without HC at different target depth	New antenna % difference in Hz field with and without HC at different target depth
1000	329	335
1500	298	305
2000	221	229
2500	160	168
3000	107	114
3500	64	68
4000	46	51
4250	12	16
4500	2	5

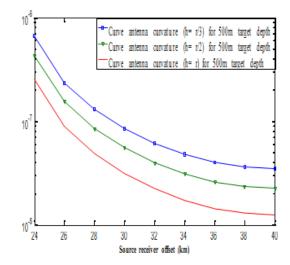


Fig. 9. Numerical model with straight antenna used for sea bed logging

Different curvatures were compared at 500m target depth in deep water environment to know which curvature gave higher signal strength with the presence of hydrocarbon reservoir. From results it was analyzed that curvature h = r/3 gave higher magnitude verses offset response as given in Figure 9.

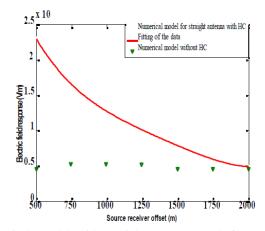


Fig. 10. Numerical model with straight antenna used for sea bed logging

C. Numerical model for straight and new antenna for deep target in deep water environment

Numerical model is a very important to know the location hydrocarbon in sea bed logging. It can provide the information about the target depth at which target depth the electromagnetic wave signal provide information about hydrocarbon reservoir. Regression analysis was done for numerical model of electric field data at different target depths. Nonlinear regression technique is used to get the best fit mathematical function for input data. Simulated data for different target depth is used for numerical model for straight and new antenna data. Guided wave response data at different target depth is used to fit the sea bed logging data for various target depths. Target depth 500m to 2000m target depth fitting of our proposed sea bed model data fitting.

Guided wave response is used for fitting the data. More than 800 data points are used for data fitting for survey area of 40kmx40km. These equations were used for numerical model. The numerical model for the straight antenna is given Figure 10. The electromagnetic field response decreases with the inverse square of the distance between the source/receiver offset. From these equations, the electric field response was calculated at far offset. At each target depth, the electric field response was used to plot the numerical model for the straight antenna. Circles represent the numerical model of the straight antenna with different target depths where as triangles without a hydrocarbon reservoir. To know the numerical model behavior again, data fitting was used which is represented by the solid line in the model. From this fitting, the general equation for the straight antenna numerical model was obtained as given (5).

$$E = \exp(cons + \alpha x + \beta x^2)$$
⁽⁵⁾

Where E is the electric field response (Ex), x is the target depth where as constants α , β represent the decay rate of guided wave from hydrocarbon reservoir and direct wave response. Decay rate of guided wave response (1.57×10-7) is slower than the direct wave response (-1.41×10-4) [27]. From this numerical model, the electric field response at different target depths can be calculated and the presence of the hydrocarbon reservoir can be predicted. At different target depths, the electric field response is given in Table 6. With the numerical model of the straight antenna, by changing the target depth it ensures that this antenna can be used to detect the 1750m target depth. Estimated electric field response with this numerical model equation also proves the accuracy of this model because at all target depths response is within the range of the with and without hydrocarbon reservoir model.

The numerical model for the curved antenna with the curvature h=r/3 was plotted with the help of data fit equations for different target depths and given (Figure 11).

$$E = \exp(cons + \alpha x + \beta x^2)$$
 (6)

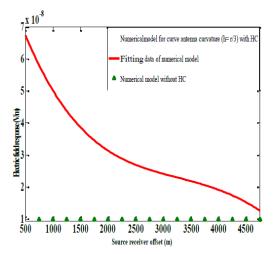


Fig. 11. Numerical model with antenna curvature h = r/3 with different target depth

Table 5.	Straight antenna E field response calculation at different target depth with the help of
	numerical model

Target depth	New antenna E field response with target depth
	(V/m)
510	$2.24 \times 10-9$
610	$1.96 \times 10-9$
710	$1.76 \times 10-9$
810	$1.56 \times 10-9$
910	1.41×10-9
1110	$1.25 \times 10-9$
1210	$1.11 \times 10-9$
1310	$1.01 \times 10-9$
1410	8.34×10-10
1510	7.53×10-10
Without hydrocarbon	4.55 × 10-10

Table 6. New antenna E field response calculation at different target depth with the help of numerical model

Target depth	New antenna E field response with target depth (V/m)
510	6.5 imes 10-8
975	5.2×10-8
1450	4.1×10-8
1925	$3.4 \times 10-8$
2400	2.8 ×10-8
2875	$2.4 \times 10-8$
3350	2.1×10-8
3825	$1.9 \times 10-8$
4300	$1.7 \times 10-8$
4775	$1.6 \times 10-8$
Without hydrocarbon	1.5 imes 10-8

Analytical results show that scattered field from hydrocarbon reservoir takes the form of exponential decay function [27]. Scattered field from hydrocarbon reservoir decay slower than the direct wave response. The equation shows the electromagnetic field behavior with target depths where x is the target depth and E the electric field response with the corresponding target depth. In equation, 5.5 Constants α , β represents the decay rate of guided and direct wave from hydrocarbon reservoir. Decay rate of guided wave response with curve antenna curvature h=r/3 (0.54×10-7) is slower than straight antenna (-1.41×10-4). The decay rate is 66% slower than straight antenna, which indicates this antenna can detect further deeper target. Different target depth

equations were plotted to get the numerical model, and it was observed that, the curved antenna with the curvature h=r/3 can detect up to a 4.5km target depth. Numerical model (Equations 5, 6) was used to validate the electric field response for straight antenna and new antenna design for

used to validate the electric field response for straight antenna and new antenna design for deep hydrocarbon target. At different target depths the electric field response from numerical model equation was within the range of electric field response as got from the simulated results. Straight and new antenna electric field response is given (Table 5, 6) respectively.

IV. Conclusion.

Electromagnetic field components response with hydrocarbon reservoir at 500m target depth was done which shows that Ex and Hz components shows better delineation than other components. Ex field response for new antenna shows 329% resistivity contrast at target depth of 1000m where as straight antenna showed 70% resistivity contrast at same target depth. Hz field shows 355% resistivity contrast where as straight antenna shows 86%. From these results it was analyzed that Hz field shows better delineation for hydrocarbon detection. It was also observed that at frequency of 0.125 Hz, new antenna gave 46% better delineation of hydrocarbon at 4000m target depth. Numerical modeling was done to know the exact target depth at which this new antenna can detect in deep water environment. It was observed that new antenna can detect 4.5 km target depth.

References

- [1] L. MacGregor, & M.Sinha, "Use of marine controlled-source electromagnetic sounding for sub-basalt exploration "Geophysical Prospecting vol. 48,1091-1106. (2000).
- [2] B.Tossman, D. Thayer, & W. Swartz, "An underwater towed electromagnetic source for geophysical exploration". IEEE Journal of Oceanic Engineering vol. 4, pp. 84-89. (1979).
- [3] S. Johansen, et al, "Subsurface hydrocarbons detected by electromagnetic sounding," first break vol. 23, pp.31-36, (2005).
- [4] Yahya N., Akhtar M.N., Nasir N., Shafie A., Jabeli M.S., and Koziol K., "CNT Fibres/Aluminium-NiZnFe₂O₄ Based EM Transmitter for Improved Magnitude vs. Offset (MVO) in a Scaled Marine Environment", Journal of Nanoscience and Nanotechnology, Accepted Article in press. 2011.
- [5] Yahya N., Akhtar M.N., Nasir N., Daud H., and Narahari M., "Forward Modeling of Seabed Logging by Finite Integration (FI) and Finite Element (FE) Methods" DSL 2011 Purtagal. Accepted Article in press. 2011.
- [6] Yahya N., Kashif M., Daud H., Zaid H.M., Shafie A., Nasir N., and See A., "Fabrication and Characterization of Y_{3.0}-xLaxFe₅O₁₂ - PVA Composite as EM Waves Detector" International Journal of Basic & Applied Sciences IJBAS Vol: 9 No: 9 131-134.
- [7] N.Nasir, N.Yahya, M.N.Akhtar, M.Kashif, A.Shafie, H.Daud, and H.M.Zaid, "Magnitude verses offset study with EM transmitter in different resistive medium," J.Applied.Sci, vol 1, (2011).
- [8] M.N.Akhtar, N.Yahya, H.Daud, A.Shafie, H.M.Zaid, M.Kashif, and N.Nasir, "Development of EM wave guide amplifier potentially used for seabed logging", J.Applied.Sci, vol 1, (2011).
- [9] M. Unsworth, "New developments in conventional hydro carbon exploration with electromagnetic methods," CSEG Recorder, pp.34-38, (2005).
- [10] P. Clemmow, "The theory of electromagnetic waves in a simple Vanisotropic medium," Proc. IEEE vol.110, pp.101–106, (1963).
- [11] FN. Kong., H. Weterdahl, Ellingsrud. S., Eidesmo. T., and Johansen S., "A possible direct hydrocarbon indicator for deep sea prospects using EM energy", Oil and Gas Journal. 100, 30-38, (2002).
- [12] C.S. Cox, S.C. Constable, A.D. Chave, S.C.Webb, "Controlled source electromagnetic sounding of the oceanic lithosphere," Nature vol. 320, pp. 52–54, (1986).
- [13] M.C.Sinha, P.D. Patel, M.J. Unsworth, T.R.E. Owen, and source electromagnetic sounding system for marine use," Marine Geophysical Research,vol. 12, pp. 29–68, (1990).
- [14] P. D. Young and C. S. Cox, "Electromagnetic active source sounding near the East Pacific Rise," Geophysical Research Letters, vol. 8, pp.1043-1046, (1981).
- [15] E. Um, & D. Alumbaugh, "On the physics of the marinecontrolled source electromagnetic method," geophysics vol.72, (2007).
- [16] S. C Webb, S. C. Constable, C. S. Cox and T. K Deaton, "A Seafloor Electric Field Instrument," Journal of Geomagnetism and Geoelectricity, vol. 37, pp.1115-1129, (1985).

- [17] A.D Chave, S.C. Constable and R. N. Edwards, "Electrical Exploration Methods For The Seafloor Electromagnetic Methods in Applied Geophysics," SEG, pp. 931–966, (1982).
- [18] T.Eidesmo, S.Ellingsrud, L.M.Mac Gregor, S.C.Constable, M.C.Sinha, S.Johansen, F.N.Kong, H.Westerdahl, "SeaBed Logging (SBL), a new method for remote and direct identification of filled layers in deepwater areas using controlled source electromagnetic sounding," First Break, vol.20, pp.144-152,(2002).